

Microreactors

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μFlow group
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Intro and objectives

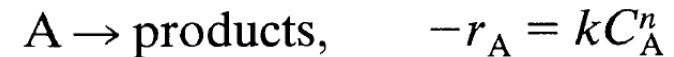
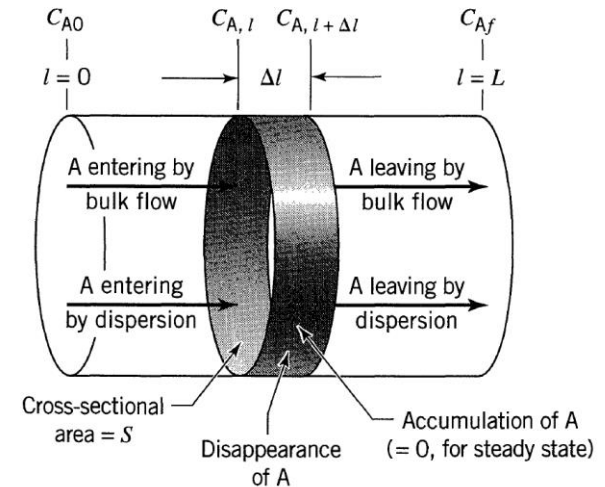
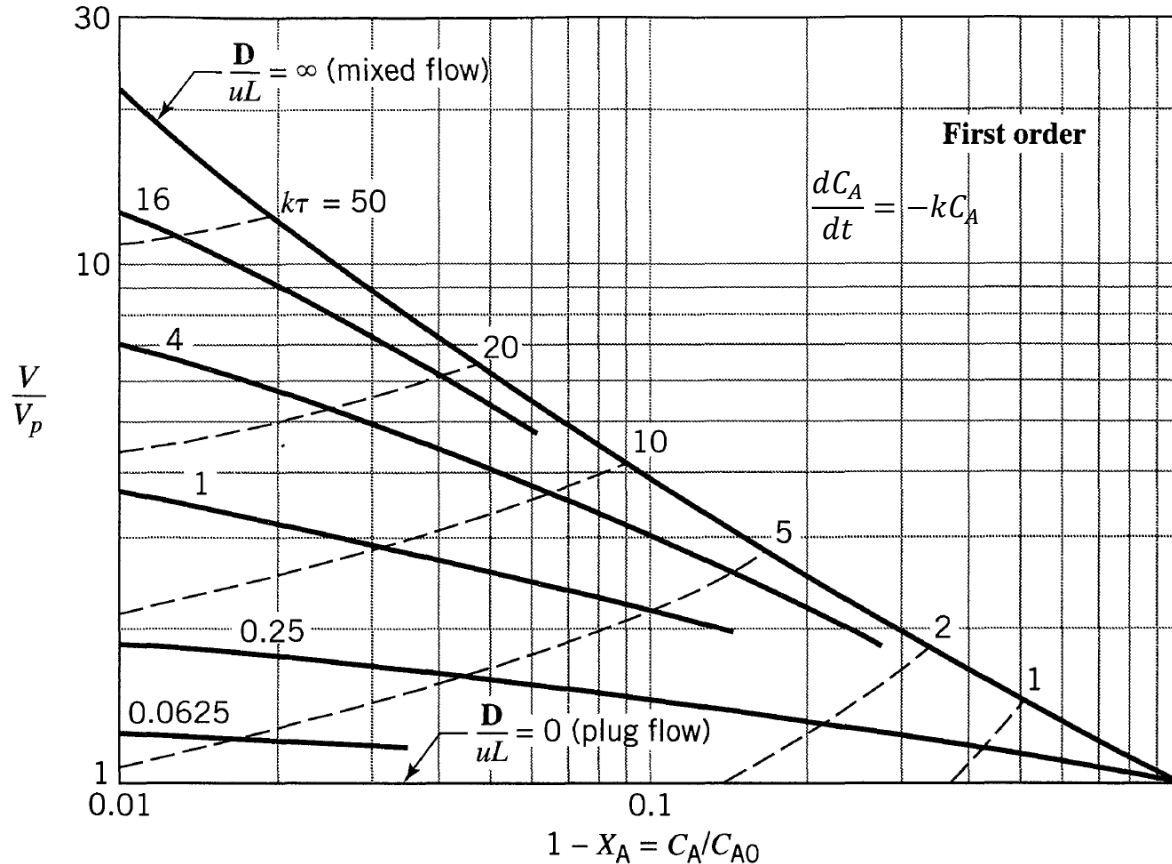
- Bio(reactors):
 - Production of/by 'particles'
 - Handling and separation of particles
 - Operate at high concentrations
- Low Re numbers advantageous?
- Throughput?
- Particle handling: small versus large particles
- Plug flow?
- Dispersion?

Outline

- Intro
 - Background
 - Fabrication
- Applications
 - Contactor: L-L-extraction
 - Heavy duty liquids crystallization
- Droplet/particle manipulation

Dispersion + reaction → higher V, t

$Bo = uL/D$



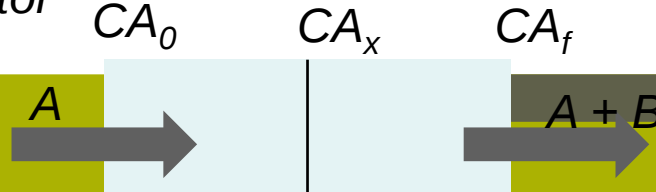
V : volume reactor (with dispersion)

V_p : volume plug flow reactor

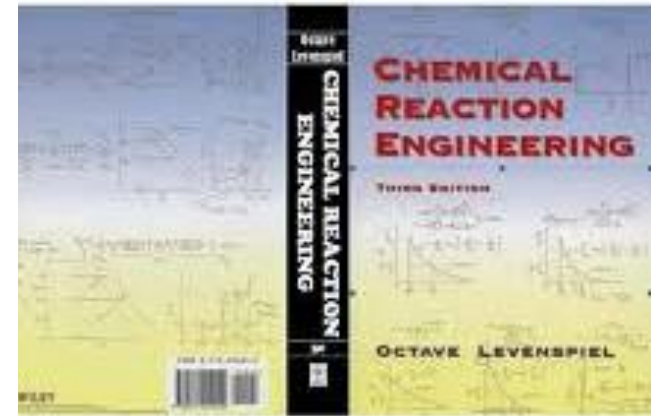
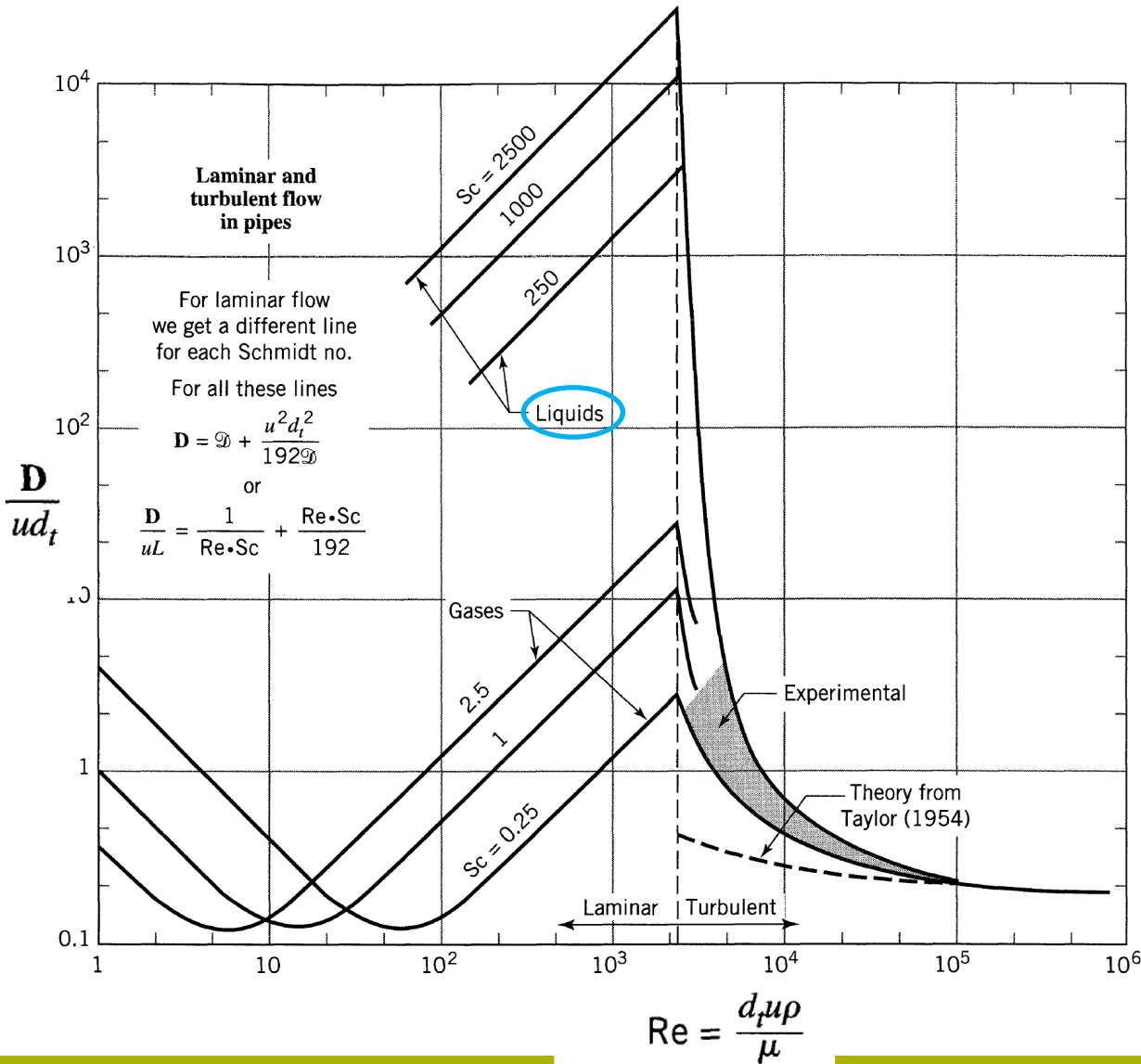
Plug flow

Chemical Reactor

Engineering, Levenspiel,
1972, Wiley



Laminar flow – turbulence in reactors



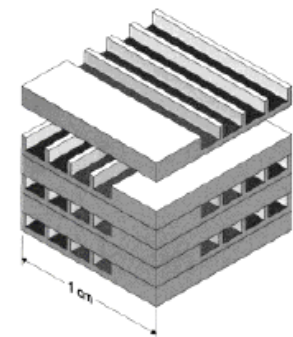
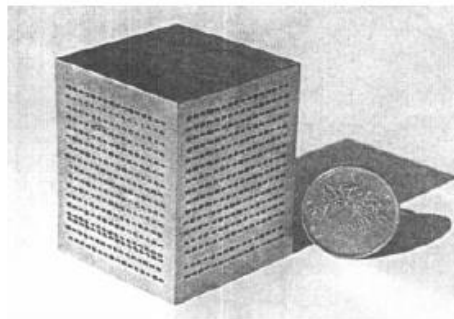
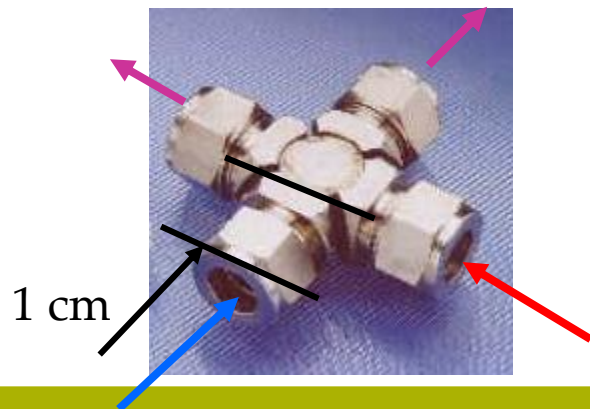
Chemical Reactor Engineering, Levenspiel, 1972, Wiley

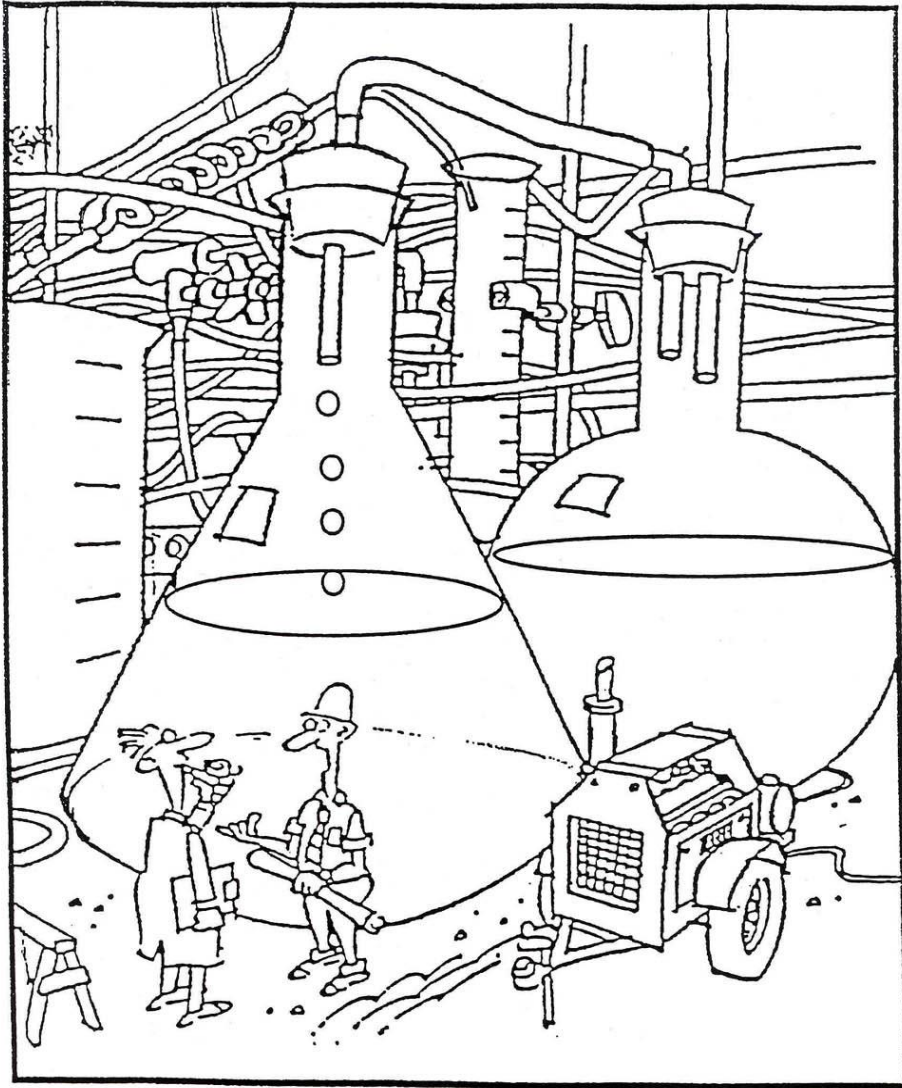
Fundamental advantages

- **Nano-scale** reactors : supra-molecular assemblies
 - Unique molecular forces due to **confinement**
 - Specific catalysts, zeolites, micelles
- **Micro-scale** reactions
 - Increase of **gradients** (T, Conc., density, pressure)
 - **Mixing** times: can be ms-ns
 - Short residence times
 - **Plug-flow**: narrow residence time distribution
 - High P-T processing: operation at liquid pressures above boiling point
 - High throughput screening of reaction kinetics
 - **Safety**
 - Scaling out

Heat aspect: Important asset of μ reactors

- More efficient and faster (**endothermic reactions**)
- No hot spots
- Controlled **exothermic reactions**: **safety!**
 - *Solvent free* processes: higher efficiency
 - Routes *in explosive regime* (actual shift: quenching of radicals by collisions with surface due to high S/V)
 - Only *small quantities* of toxic or explosives required ($\leftrightarrow$ batch reactors)





Upscaling is not
always
straightforward

"It worked fine in the lab !"

Reactor upscaling



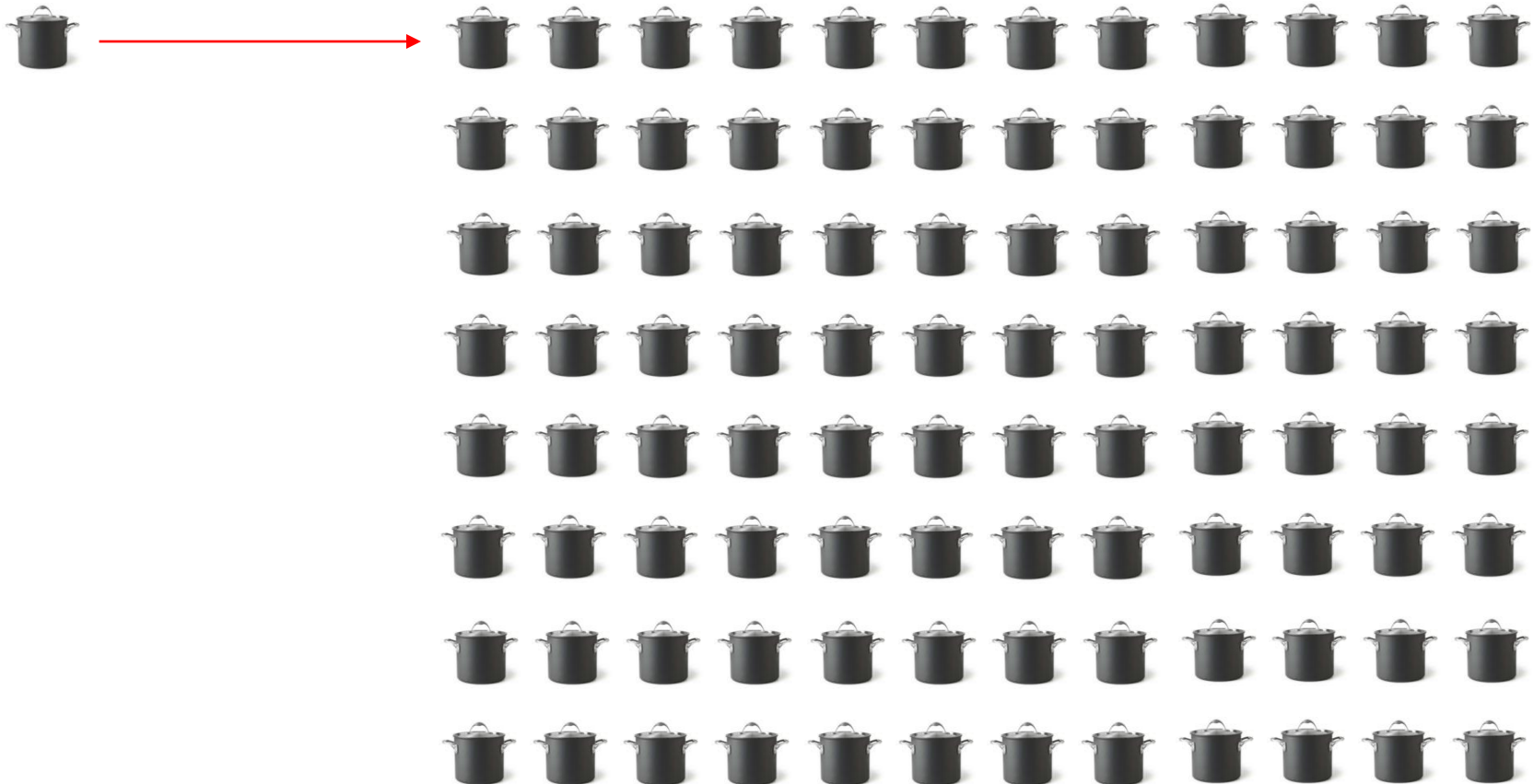
Small lab beaker



Industrial tank



Reactor replication ("numbering up")



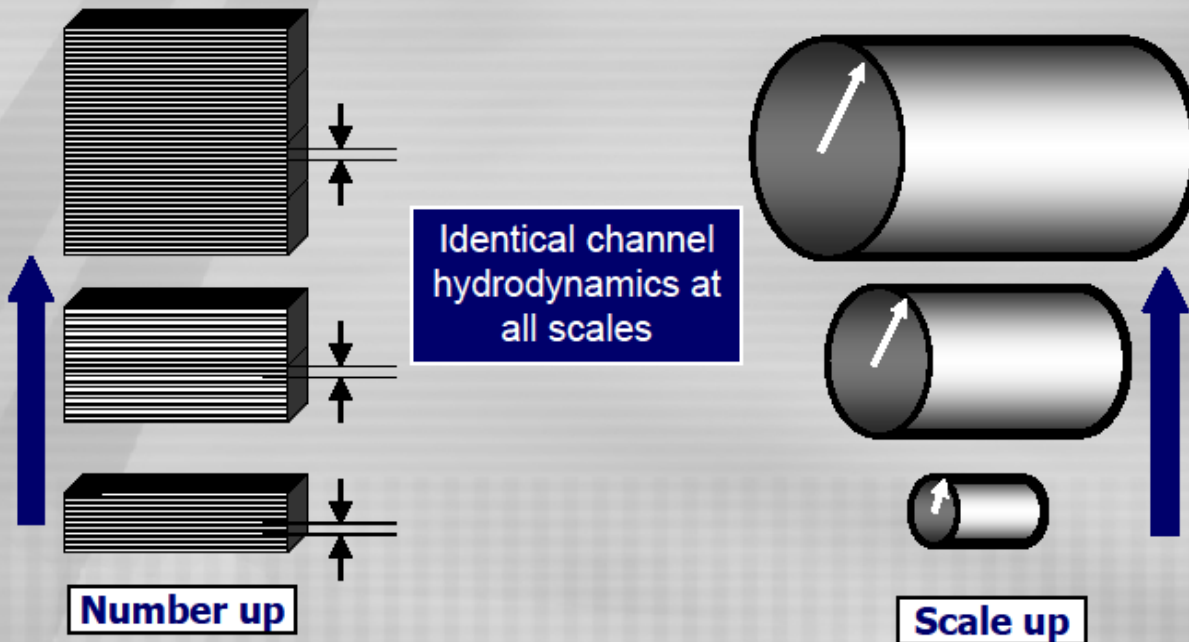
Numbering up vs. scaling-up

Scaleable:

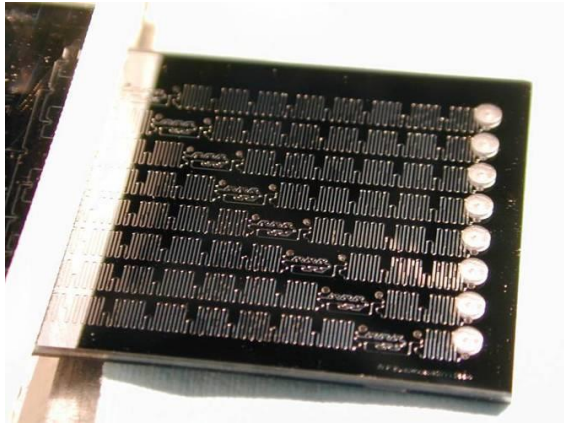
“Numbering-up” vs Scaling-up



Reduce time and cost to commercialization



Micro-reactor scales



1 mg/hr



1 kg/hr



1700 kg/hr

Ammonium nitrate - 1921



BASF, Oppau/Ludwigshafen,
September 21, 1921

Killing 500–600 people and injuring about 2,000 more

Ammonium nitrate is **strongly hygroscopic**, so the mixture of **ammonium sulfate and nitrate clogged together** under the pressure of its own weight, turning it into a **plaster-like** substance in the 20 m high silo.

The workers needed to use pickaxes to get it out, a problematic situation because they could not enter the silo and risk being buried in collapsing fertilizer.

To ease their work, **small charges of dynamite were used to loosen the mixture**. The procedure was tried experimentally and was considered safe. It was not known at the time that ammonium nitrate was explosive.

A theory is that the mixture changed and a higher concentration of ammonium nitrate was present.

Ammonium nitrate - 2001



Ammonium nitrate decomposes in temperatures above 210 °C. **Pure AN is stable and will stop decomposing once the heat source is removed, but when catalysts are present** (combustible materials, acids, metal ions, chlorides. ..) **the reaction can become self-sustaining** (known as self-sustaining decomposition, SSD).

The exact cause of this disaster remains unknown.

AZF, Toulouse,
September 21, 2001

Minifactories: "smaller=safier"



An expensive lesson:

Accident at Bhopal, 1984

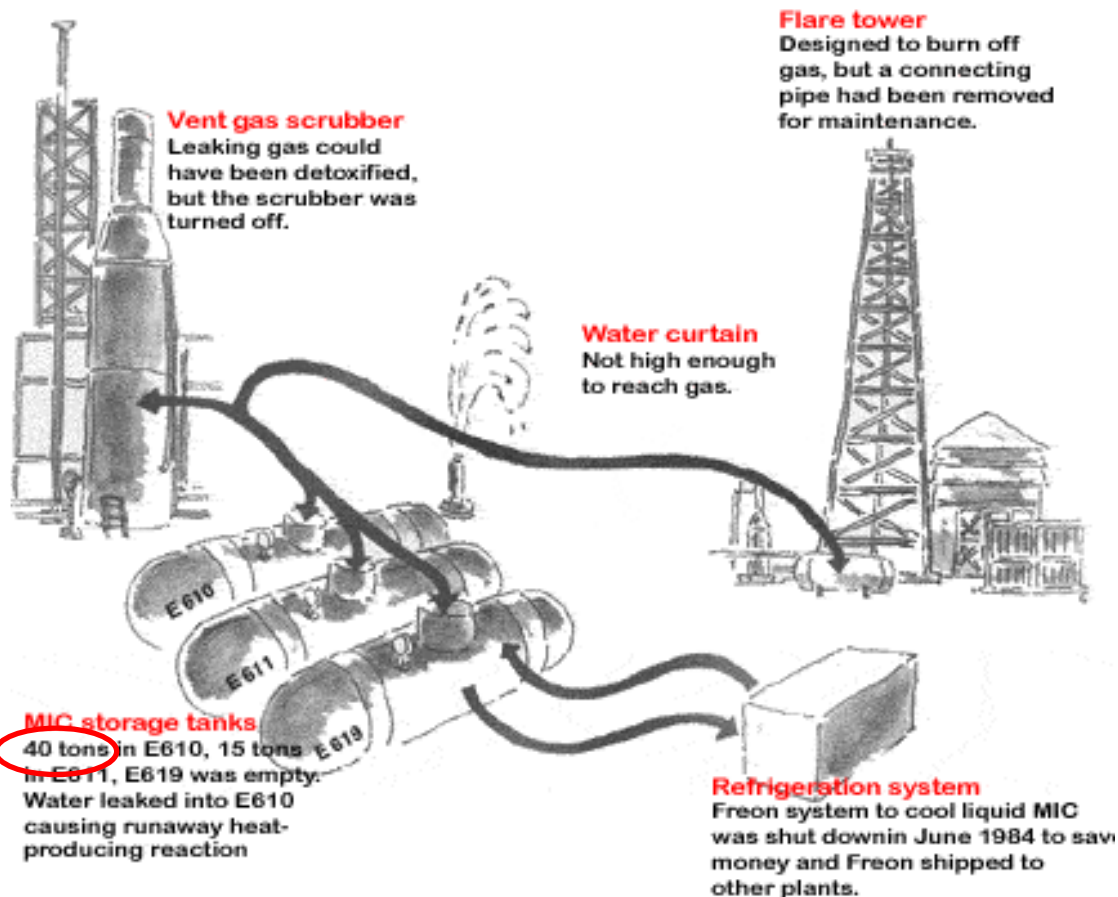
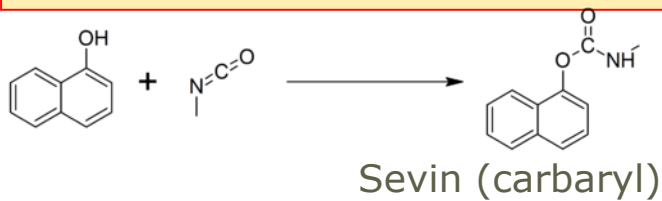
To produce the pesticide Sevin

>50,000 injured (>2000 casualties, long-term 10,000) run-away reaction and escaped toxic gas

Proces-intensified continuous reactors could have processed MIC* directly with less than 10 kg MIC present

*methyl isocyanate

D.C. Hendershot, Chem. Eng. Progr, Jan. 2000, p. 35



Water entered a tank containing 42 tons of MIC.

The resulting exothermic reaction increased the temperature inside the tank to over 200 °C (392 °F) and raised the pressure. The tank vented releasing toxic gases into the atmosphere

Amm. nitr. accidents during transport

Port Neal, Iowa, 1994

[[edit](#)]

- At about 6:13am on December 13, 1994, two explosions rocked the Port Neal, Iowa ammonium nitrate processing plant operated by Terra Industries. Four people were killed and 18 injured. Approximately 5,700 tons of anhydrous ammonia were released and releases of ammonia continued for six days after the explosions. Groundwater under the processing plant was contaminated by chemicals released as a result of the blast. The timing of the explosion occurred prior to the start of the arrival of the 8:00am shift personnel, or the death toll may have been larger.^{[1][2]}

Toulouse, France, 2001

[[edit](#)]

Main article: [AZF_\(factory\)](#)

- On September 21, 2001, at 10:15 AM, in the [AZF_\(factory\)](#) (Azote de France) fertiliser factory in [Toulouse, France](#), an explosion occurred in a warehouse where the off-specification granular AN was stored flat, separated by partitions. About 200–300 tons is said to be involved in the explosion, resulting in 31 people dead and 2,442 injured, 34 of them seriously. The blast wave shattered windows up to 3 kilometres away and the resulting crater was 10 metres deep and 50 metres wide. The exact cause remains unknown. The material damage was estimated at 2.3 [billion euros](#).

Cartagena, Murcia, Spain, 2003

[[edit](#)]

- The fertilizer storage facility of Fertiberia held a self sustained decomposition (SSD) fire in January 2003. The fire was controlled after most of the material was removed by mechanical means.

Barracas, Spain, 2004

[[edit](#)]

- A truck carrying 25 tonnes of ammonium nitrate fertilizer exploded half an hour after a traffic accident on March 9, 2004, killing two people and injuring three others. The explosion, which could be heard at a distance of 10 km (6.2 mi) caused a crater five metres deep.

Mihăilești, Buzău, Romania, 2004

[[edit](#)]

Main article: [Mihăilești explosion](#)

- A truck carrying 20 tones of ammonium nitrate tipped over and caught fire. The fire started in the cabin. Two reporters got to the site of the accident and started filming while firemen were trying to stop the fire. Around 42 meters in diameter was formed by the explosion.

Ryongchŏn, North Korea, 2004

[[edit](#)]

Main article: [Ryongchon disaster](#)

- A freight train carrying ammonium nitrate exploded in the station, destroying over 3000 others. The station was destroyed, as were most buildings within 500 metres, and nearly 8000 homes were destroyed or damaged. Two craters of about ten metres in depth were seen at the site of the explosion. The authorities blamed "human error" for the explosion, although rumours persist that it was in fact an attempt to assassinate the Korean leader [Kim Jong-il](#), who was due to be passing through the station at the time.

Estaca de Bares, Spain, 2007

[[edit](#)]

- The NPK fertilizer cargo of the ship [Ostedijk](#) sustained a self sustained decomposition (SSD) fire for 11 days. The fire plume reached 10 m in diameter and several hundred meters in length. Special water spears were inserted inside the cargo to extinguish the fire.

Monclova, Coahuila, Mexico, 2007

[[edit](#)]

- On September 10, 2007 near Monclova, Coahuila, México, a trailer loaded with 22 tons of ammonium nitrate crashed into a truck leaving three dead in the crash. A fire then started in the trailer's cabin and approximately 40 minutes after that, a huge explosion occurred, resulting in around 150 people injured and 37 more dead. A crater 30 ft (9.1 m) wide and 6 ft (1.8 m) deep was created due to the explosion.^[12]

Bryan, TX, United States, 2009

[[edit](#)]

- A plant in Bryan, TX (El Dorado Chemical Company) which processes ammonium nitrate into fertilizer, caught fire at about 11:40 am on July 30, 2009. Over 80,000 residents in the Bryan/College Station area were asked to

Distributed
production !!!

Central or distributed ?



1965



2000



2000



2018 ?

"The natural course of every technology leads to fragmentation and smallness."

George Gilder, Harvard Business Review, April 1988

"We are blocking our roads with trucks..... Decentralization burdens the environment much less"

interview with Jos Put, CTO DSM, in C₂W, 15 Sept. 2007

Industrial preactor, DSM Linz, 2005



65 cm, 290 kilo

1700 kg liquid/h

Removes a few 100 kW reaction heat

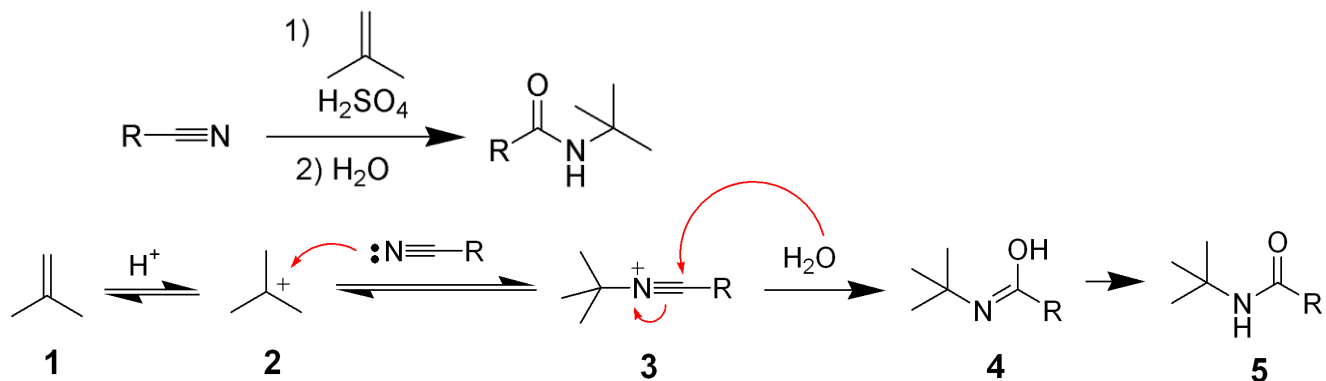
Contains mixers and a few thousand of microchannels

production: 300 ton in 10 weeks

Developed by Forschungszentrum Karlsruhe (FZK) and DSM

Specific aspects reaction

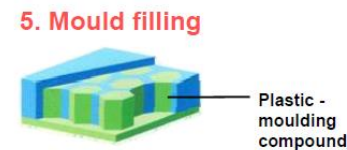
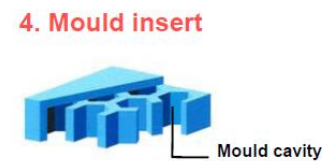
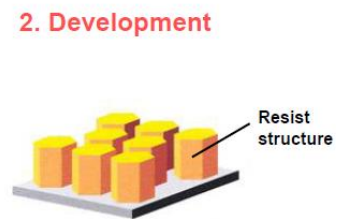
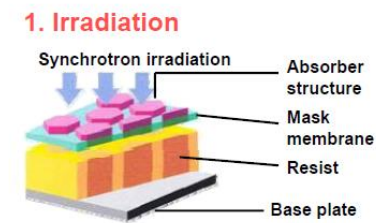
Goal was: synthesis organic intermediate via "Ritter" reaction:



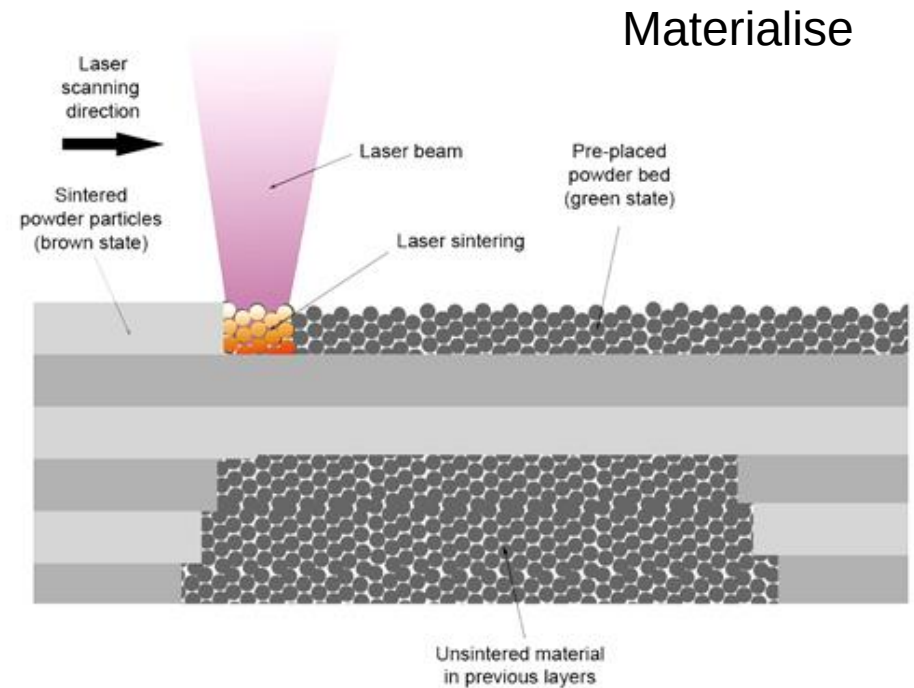
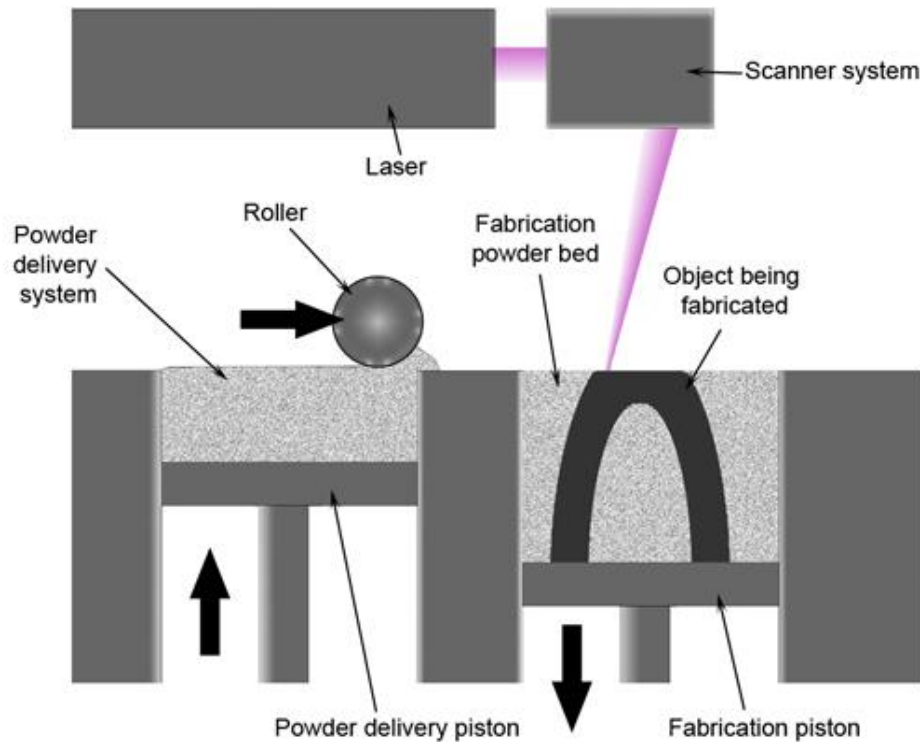
- Very **fast** reaction
- Highly **exotherm**
- **Toxic products**, concentrated sulfuric acid
- Large differences in and **fast increase of viscosity**

LIGA (Lithography, Galvanoformung, Abformung)

- Lithographic step (laser, electron- or ion beam, UV, X-ray: large AR's)
- Electroplating
- Mold insert or embossing: replication
 - mass production of plastics
- High precision, high surface quality, high AR's
- Based on broad material palette:
 - Metals: direct
 - Ceramics: cast
 - Polymers: cast



Laser melting deposition

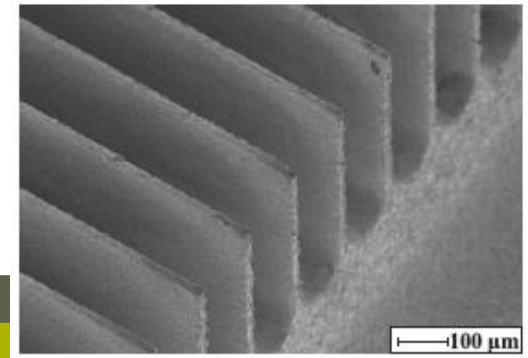
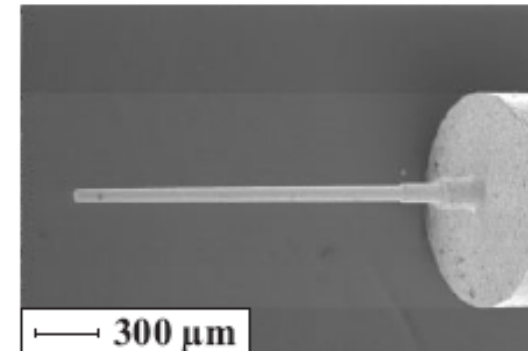
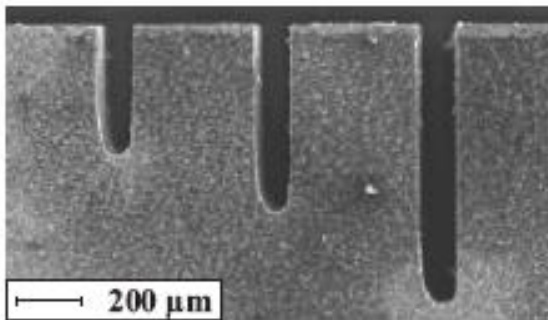


Materialise

	SLM 250	SLM 125
Build volume	250mm x 250mm x 300mm (x,y,z) z extendable to 400mm	125mm x 125mm x 125mm (x,y,z)
Fiber laser power	200 – 400 W	100 – 200 W
Layer thickness	20 to 100µm	20 to 100µm
Standard laser spot size	50 microns diameter at powder surface	30 microns diameter at powder surface
Available materials	Stainless Steel 316L and 17-4PH, H13 Tool Steel, <u>Aluminium</u> Al-Si-12Mg and Al-Si-10Mg, <u>Titanium</u> CP, Ti-6Al-4V and Ti-6Al-7Nb, <u>Cobalt-Chrome</u> (ASTM75), Inconell 718 and 625	

Electro-discharge machining

- Especially appropriate for hard or chemically resistive materials
- Can be applied on all kinds of **conductive materials**
- Voltage generator, electrode
- Technology based on **erosion process: discharge** between electrode and workpiece
- Advantages
 - **No mechanical contact: no contamination**
 - 3D machining possible (vs. 2.5 D)

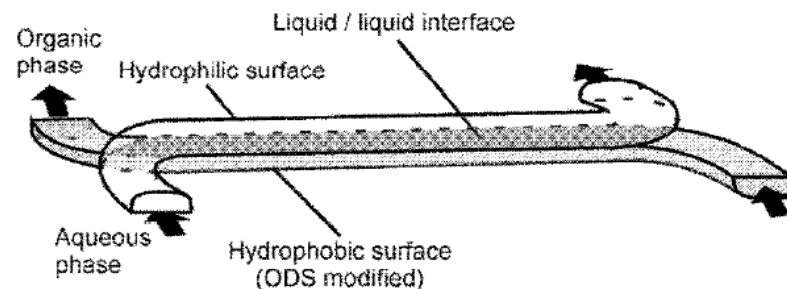
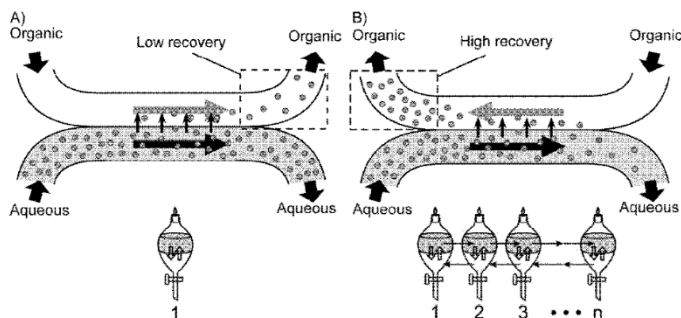


CONTACTING LIQUIDS

On-chip contactor/extractor

- Need for small scale extraction units
 - sample preparation
 - small scale production of pharmaceuticals
 - process development
- Increasing demand to combine extraction with reaction, heat transfer, (photo)catalysis, etc.
- Phase separation often slowest step: demand for alternative configurations

Interface stabilization



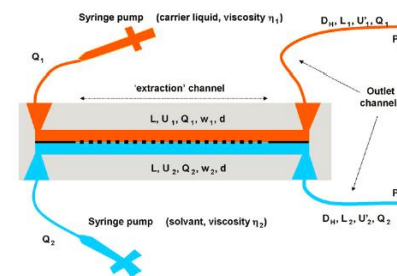
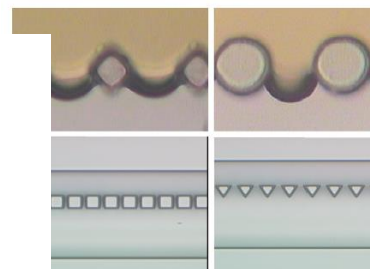
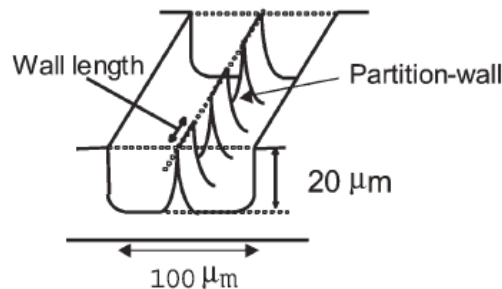
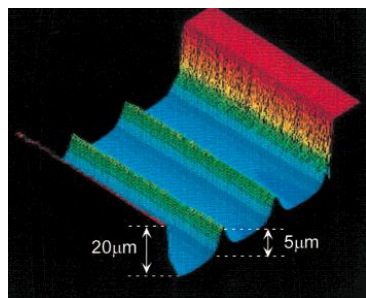
MICRO COUNTER-CURRENT FLOW SYSTEM FOR HIGHLY EFFICIENT EXTRACTION

A. Aota¹, M. Nonaka¹, A. Hibara¹ and T. Kitamori^{1,2}

¹Department of Applied Chemistry, School of Engineering, The University of Tokyo

²Kanagawa Academy of Science and Technology (KAST)

7th International Conference on Miniaturized Chemical and Biochemical Analysis Systems
October 5–9, 2003, Squaw Valley, California USA



The physics of a coflow micro-extractor: Interface stability and optimal extraction length

J. Berthier*, Van-Man Tran, F. Mittler, N. Sarrut

Anal. Chem. 2002, 74, 1565–1571

Continuous-Flow Chemical Processing on a Microchip by Combining Microunit Operations and a Multiphase Flow Network

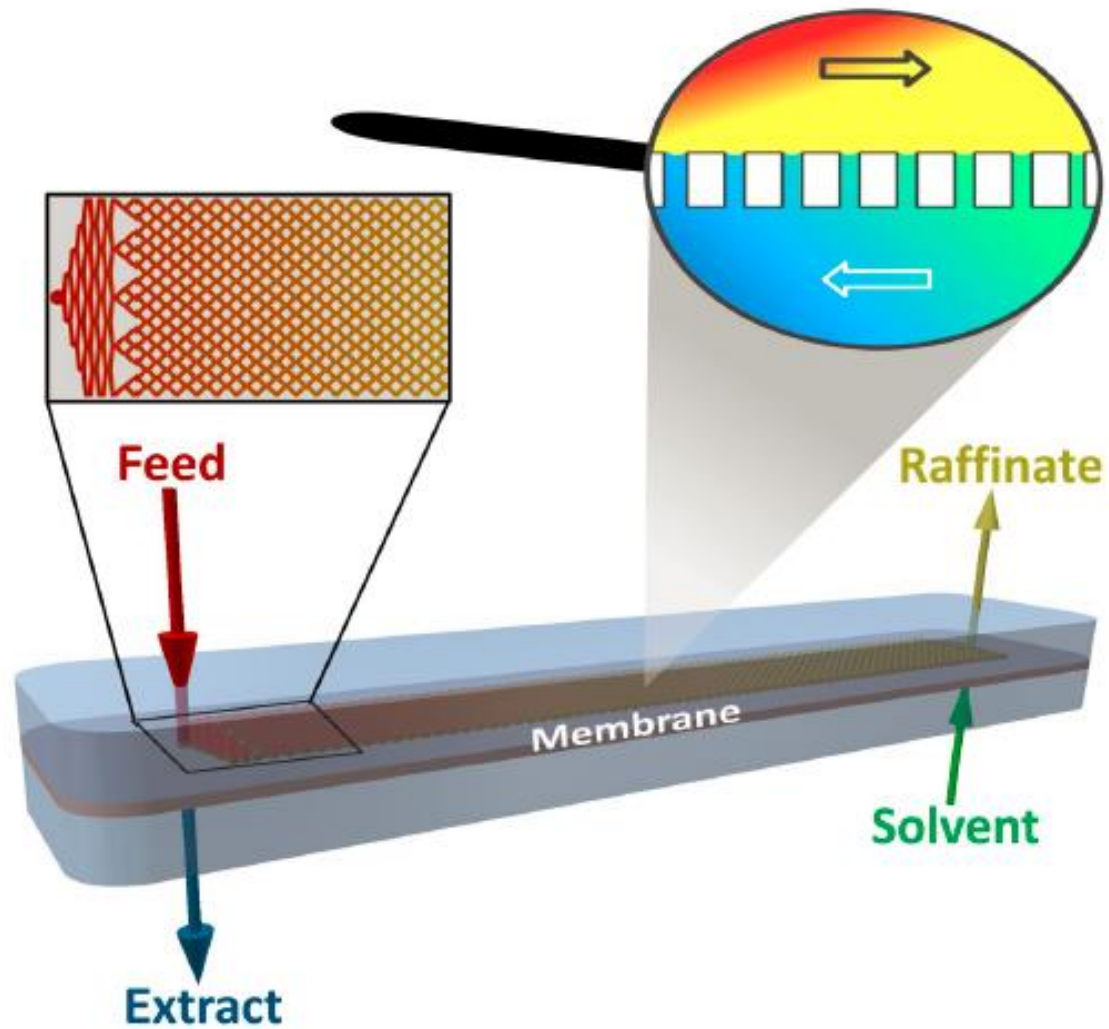
Manabu Tokeshi,¹ Tomoko Minagawa,² Kenji Uchiyama,² Akihito Hibara,² Kiichi Sato,² Hideaki Hisamoto,² and Takehiko Kitamori^{1,2}

Intermittent partition walls promote solvent extraction of metal ions in a microfluidic device

Tatsuo Maruyama,^a Tomoaki Kaji,^a Tomohiro Ohkawa,^b Ken-ichiro Sotowa,^a Hironari Matsushita,^a Fukiko Kubota,^a Norihiro Kamiya,^a Katsuki Kusakabe^a and Masahiro Goto^{a*}

Sensors and Actuators A 149 (2009) 56–64

Membrane contactor



Membrane contactor (co-current)

- 1.3 cm wide channel

- Flow distribution
- Support structures
- 100 μm deep channels
- 70 μm thick membrane



$$\Delta P_{Laplace} = -\frac{2\gamma\beta \cos \theta}{r}$$

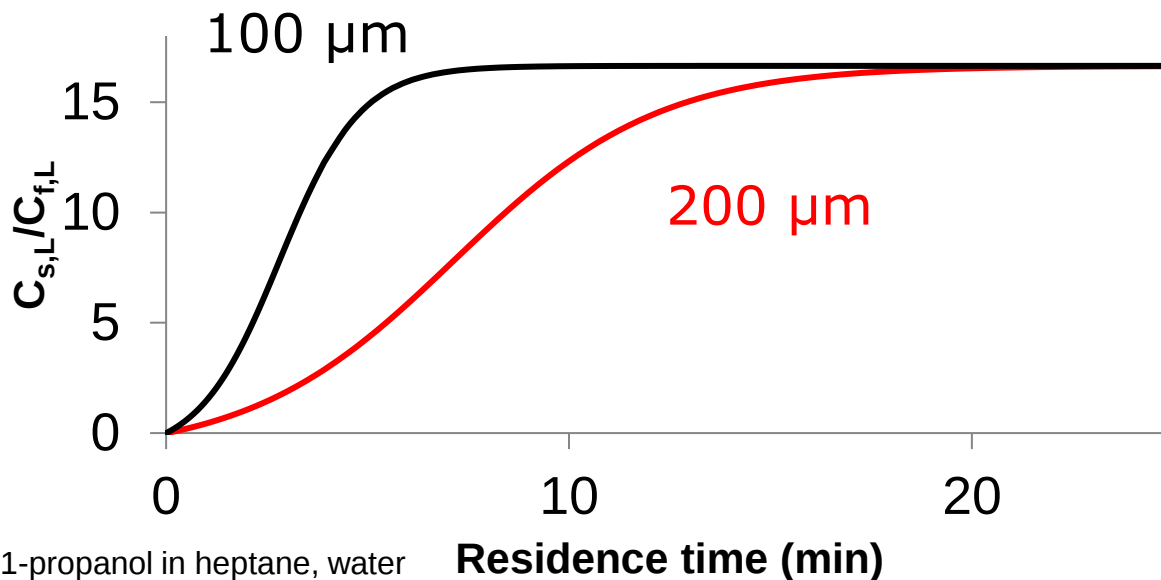
γ = Interfacial tension

β = Pore shape factor ($0 < \beta < 1$)

θ = Contact angle

(Membrane/Liquid 1/ Liquid 2)

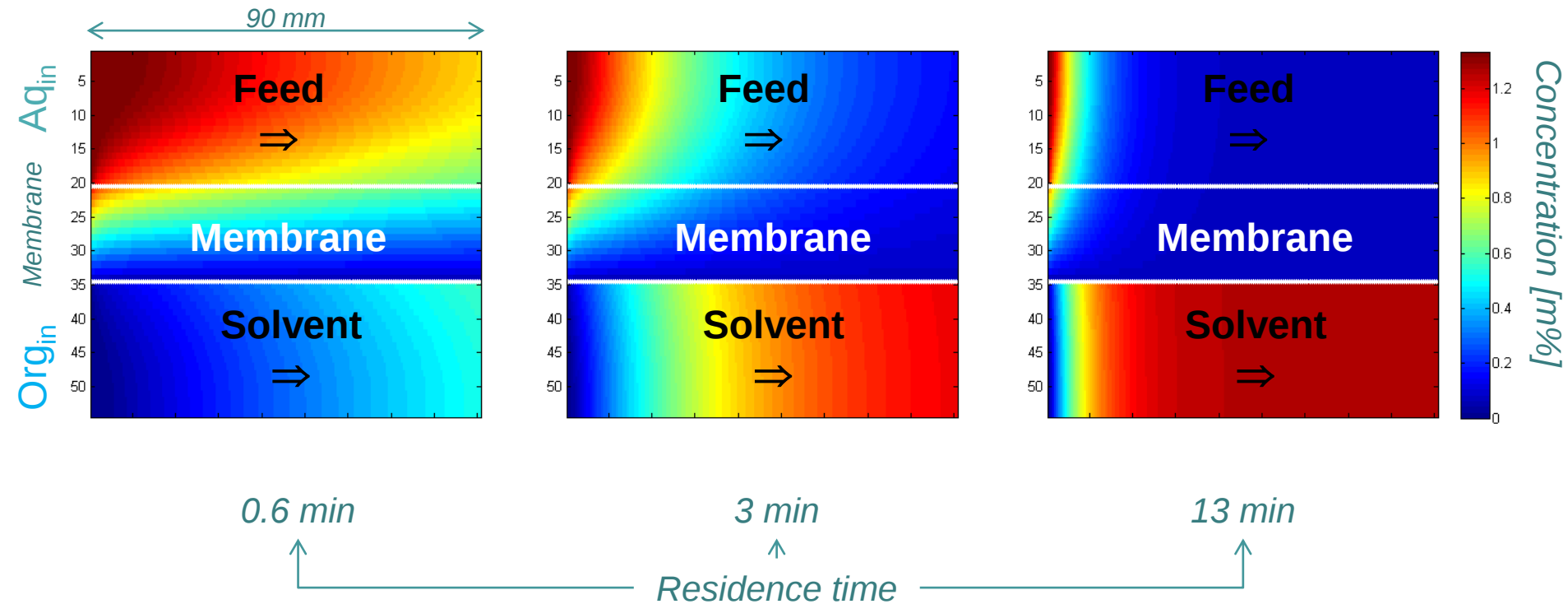
r = pore radius



$$\frac{C_{s,L}}{C_{f,L}} = \frac{1 - e^{-\frac{KL}{u_f h_f} \left(1 + \frac{\alpha_f}{\alpha_s}\right)}}{\frac{\alpha_s}{H \alpha_f} e^{-\frac{KL}{u_f h_f} \left(1 + \frac{\alpha_f}{\alpha_s}\right)} + \frac{1}{H}}$$

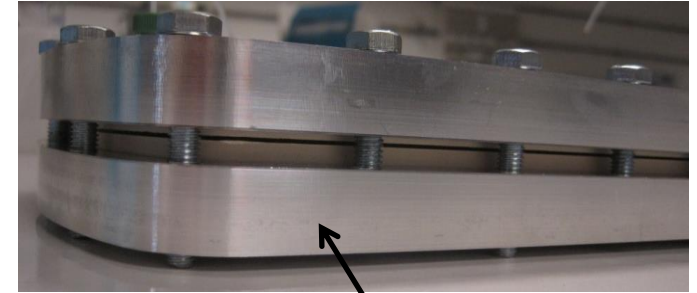
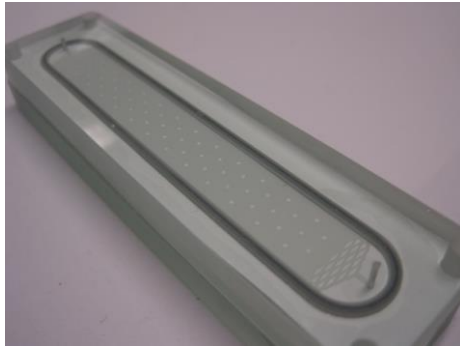
$$\alpha_f = \frac{u_f h_f}{KL} \quad \alpha_s = \frac{u_s h_s H}{KL}$$

Kinetics

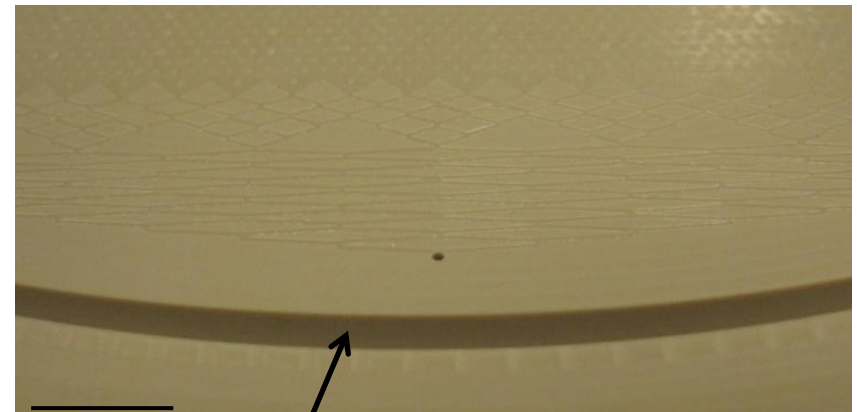


Contactors configuration

Glass, PMMA, PEEK, POM, Alu



rigid casing for plastic substrates



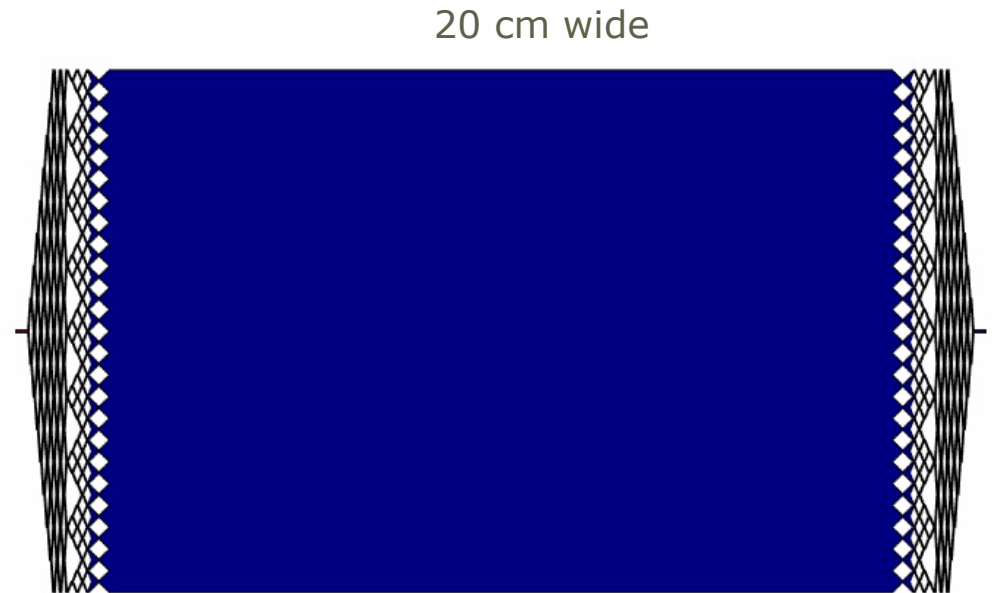
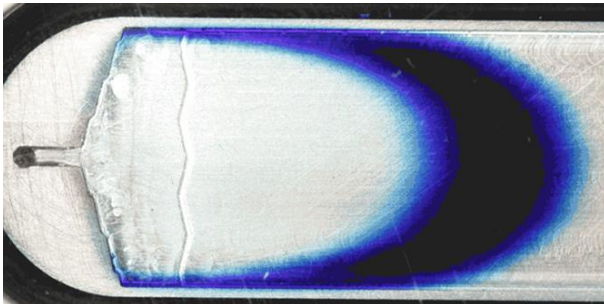
1 cm

sealing

10 cm

Membrane contactor: increasing throughput

- Distributor
- Straightforward increase in width

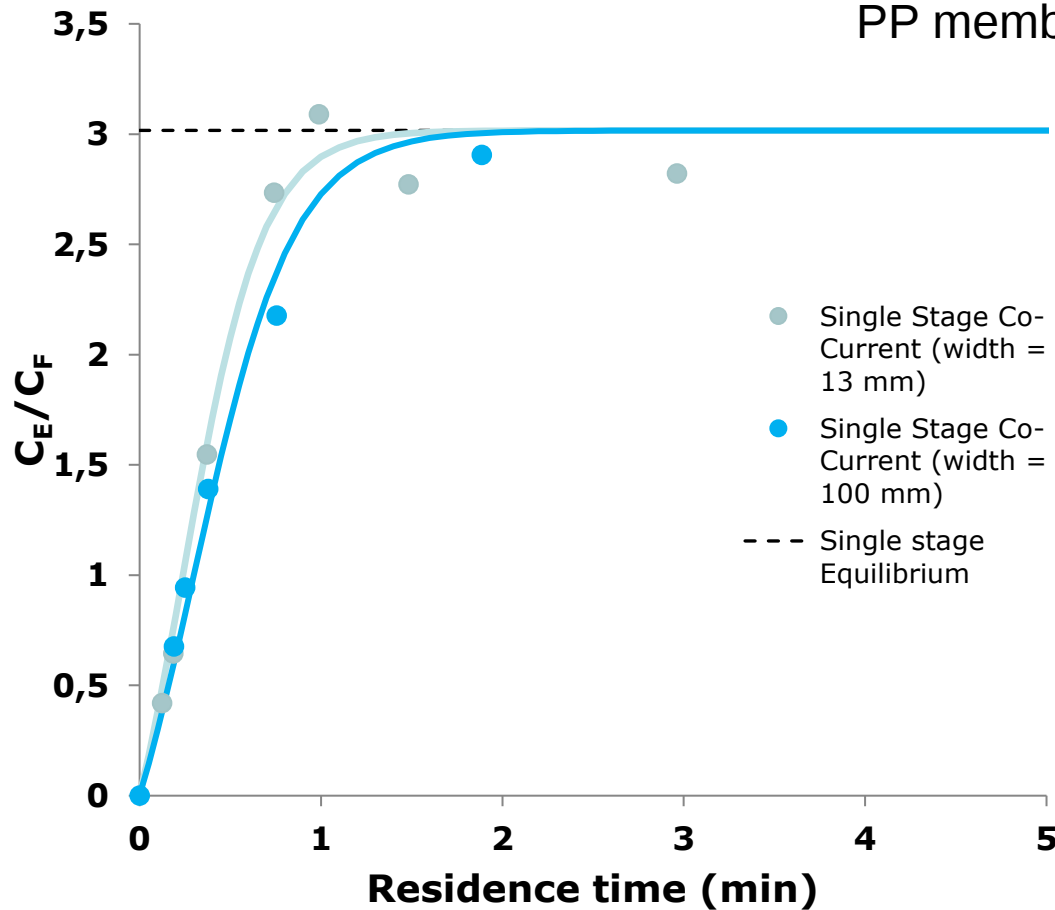


From 1.3 cm to 10 cm

Feed: Heptane+3% benzylalcohol

Solvent: water

PP membrane 20 μm thick



10 cm wide channel

$V=1$ ml

$F: 1$ ml/min

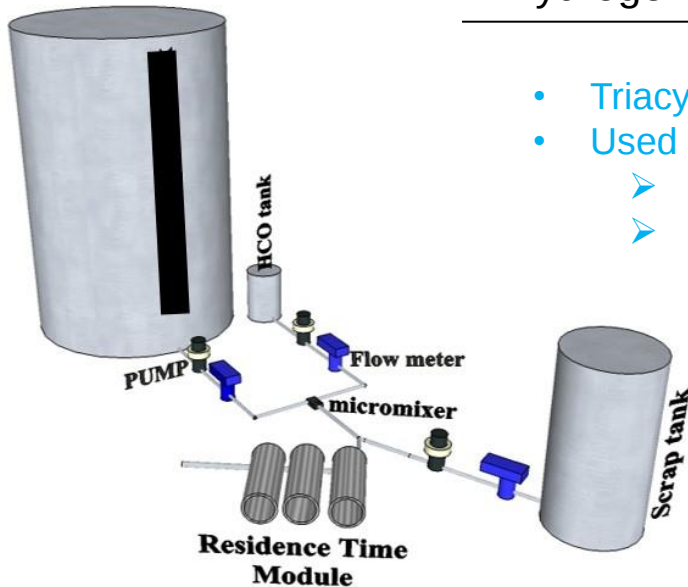
CRYSTALLIZATION

Emulsion crystallization of HCO

P&G

I. Hydrogenated castor oil (HCO)

- Triacylglycerol (fat)
- Used in heavy duty liquids
 - Prevents phase split
 - Increases the viscosity



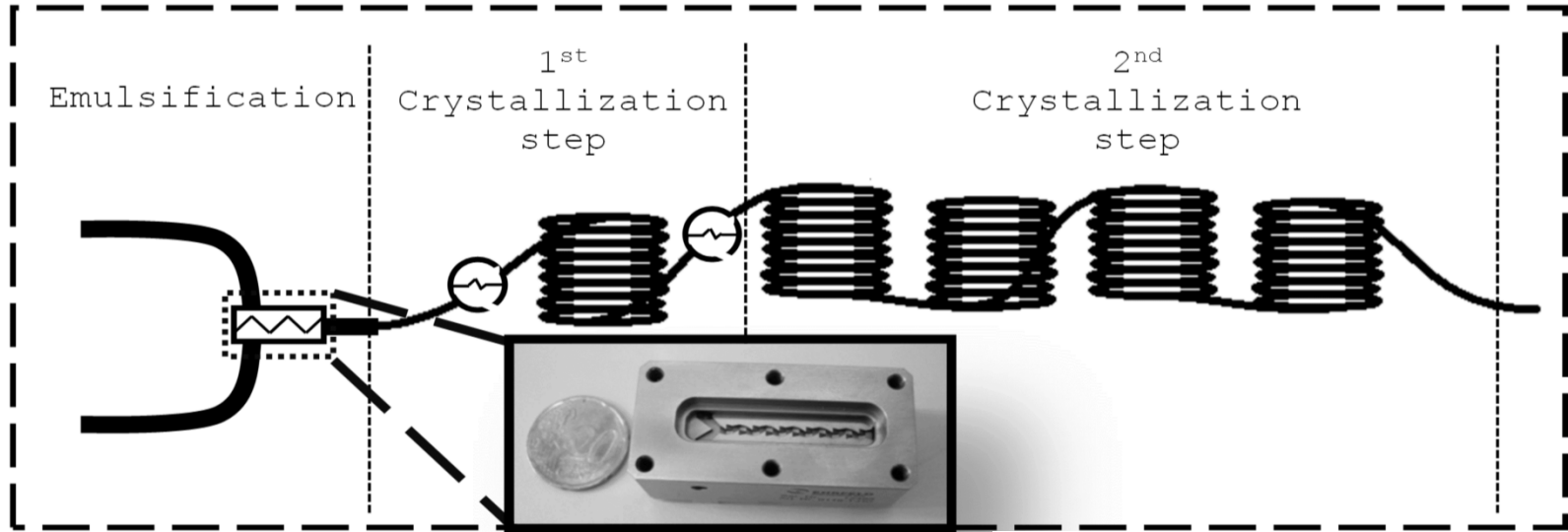
II. Meso-micro continuous process designed for the crystallization of Hydrogenated Castor oil (HCO)

- Ehrfeld microreactors & Swagelok tubing
- Total flow **5 – 20 kg/h**

III. Main objectives

- Increasing performance by **controlling the crystal shape**
- Characterization of the emulsion crystallization

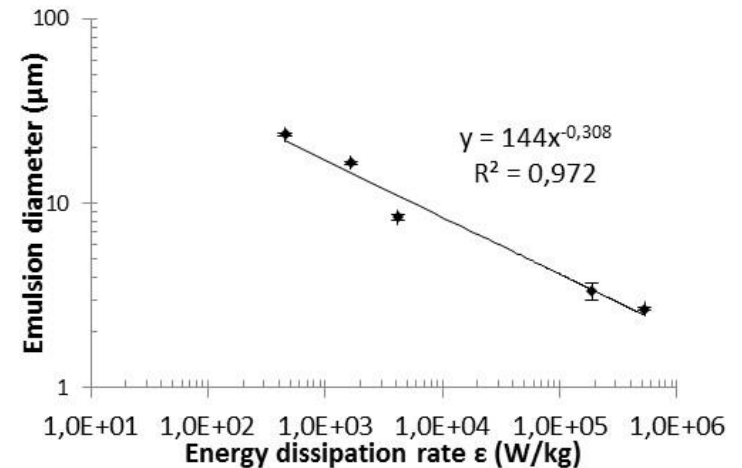
Emulsion crystallization of HCO



III. The emulsion crystallization of HCO

Contains two transformation steps

- Part I: **Emulsification**
- Part II: **Crystallization**



Emulsion crystallization of HCO

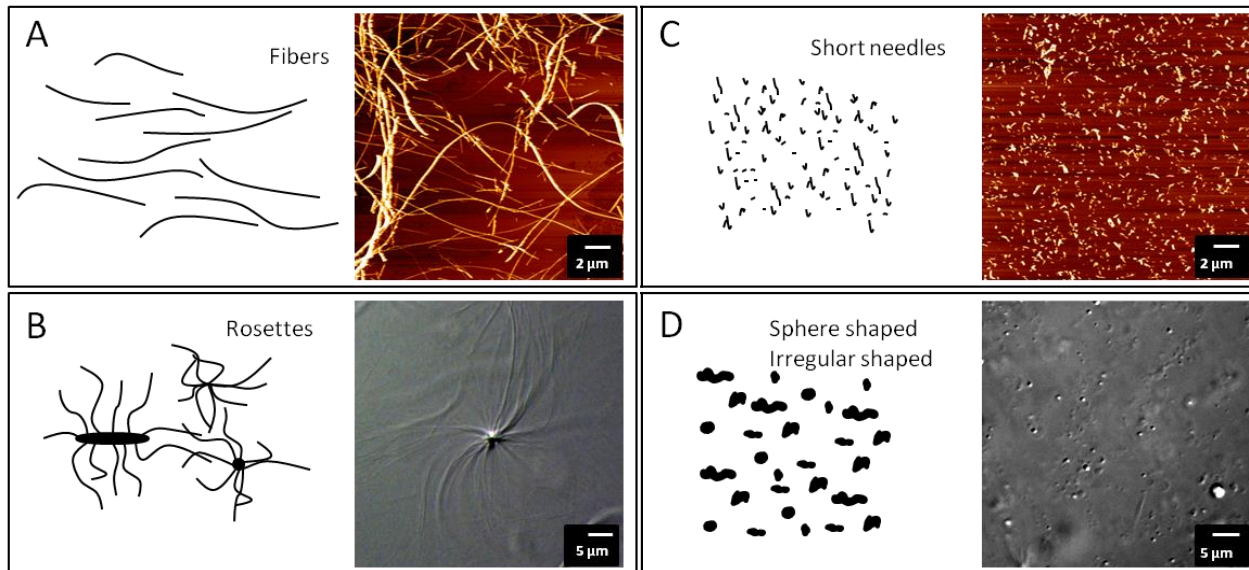
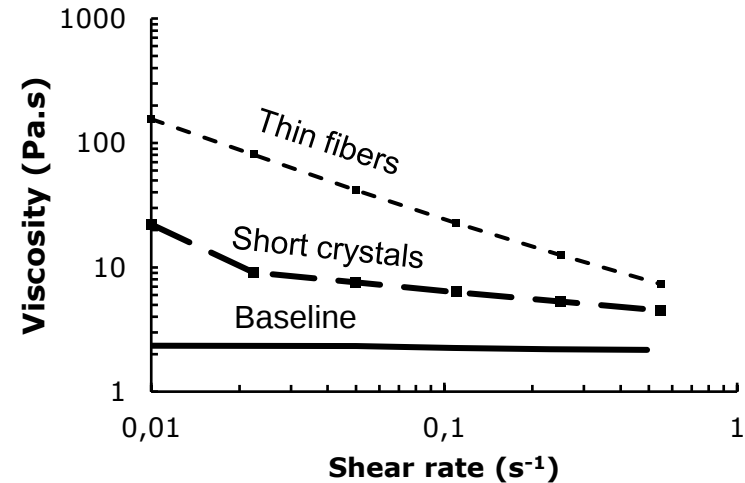
Crystallization - Crystal shape

Which crystal shape do we want?

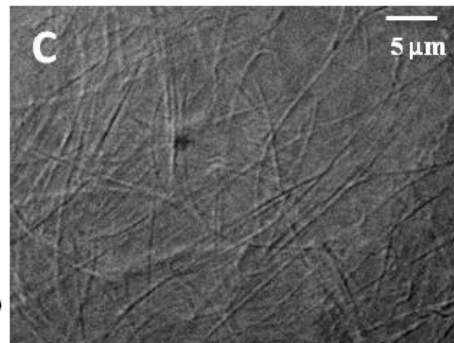
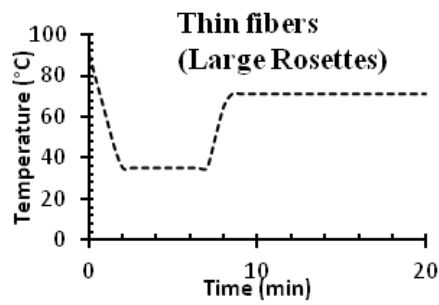
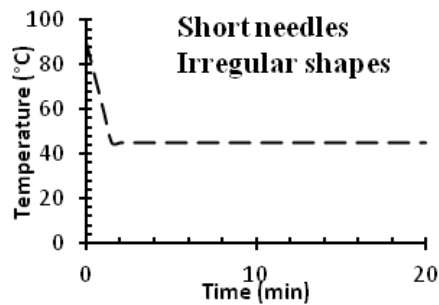
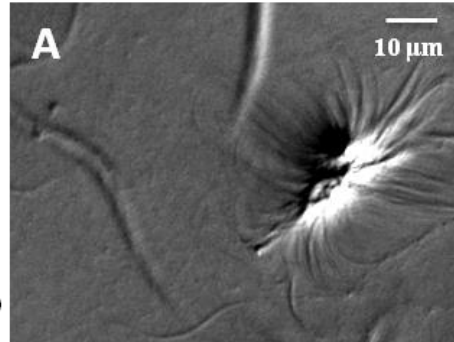
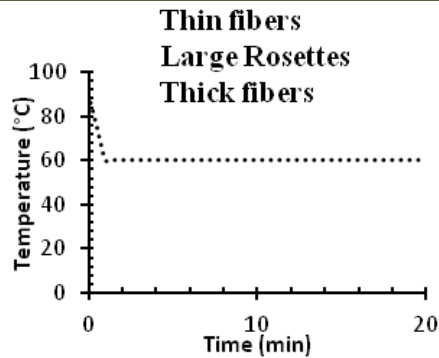
→ Thin fibers

Why?

→ The highest low-shear viscosity increase



Emulsion crystallization of HCO



Identifying the optimal process parameters

Temperature

- $T > 60\text{ }^{\circ}\text{C}$
Large rosettes and fibers
- $T < 60\text{ }^{\circ}\text{C}$
Short needles and irregular shapes
- $T_1\ 33\text{ }^{\circ}\text{C} - 45\text{ }^{\circ}\text{C} // T_2\ 71\text{ }^{\circ}\text{C}$
Thin fibers

Emulsion size

Shear rate

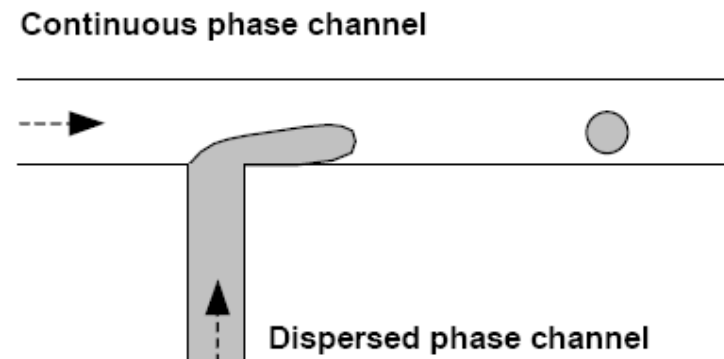
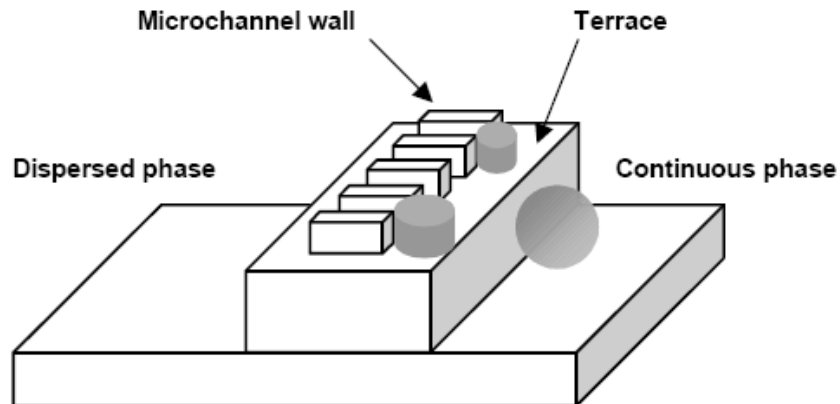
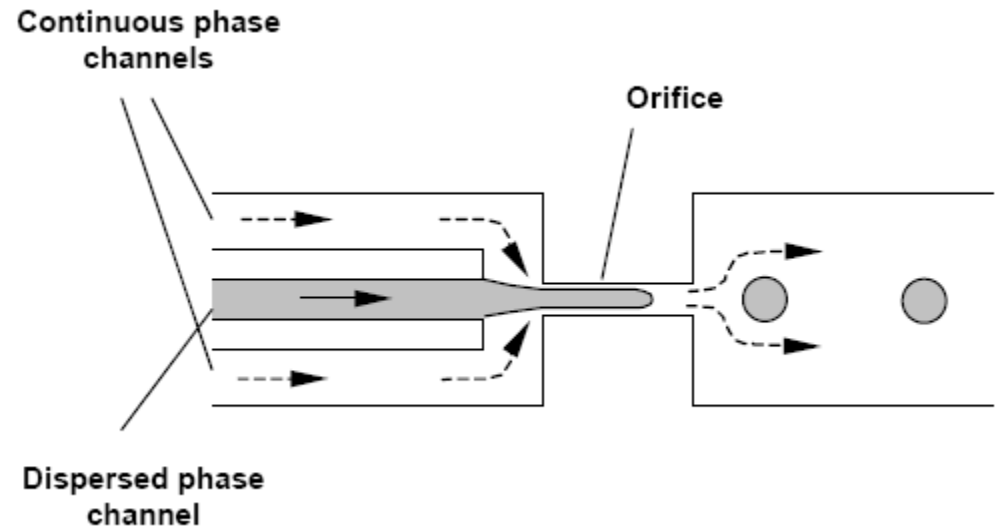
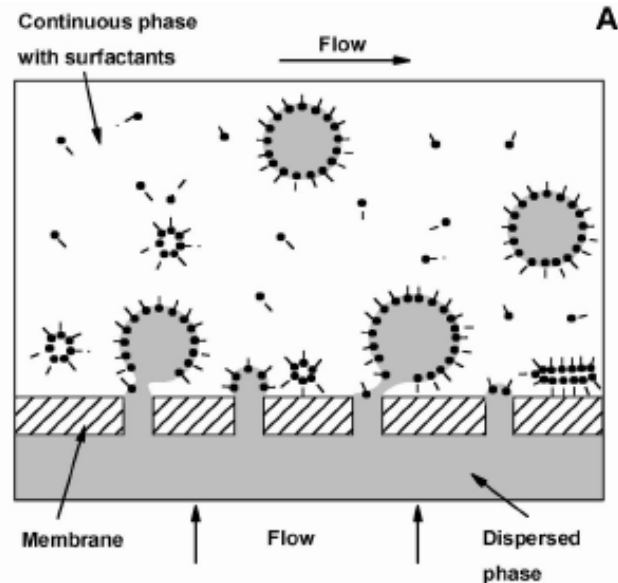
[Surfactant]

[HCO]

Etc...

DROPLET GENERATION AND MANIPULATION

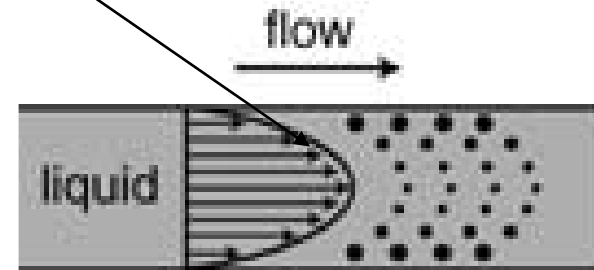
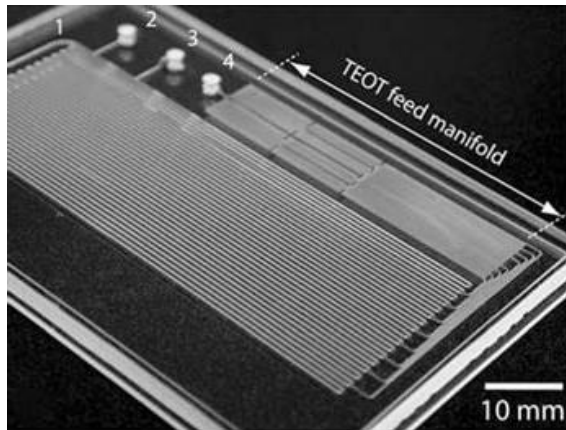
Emulsification using specific channel geometries



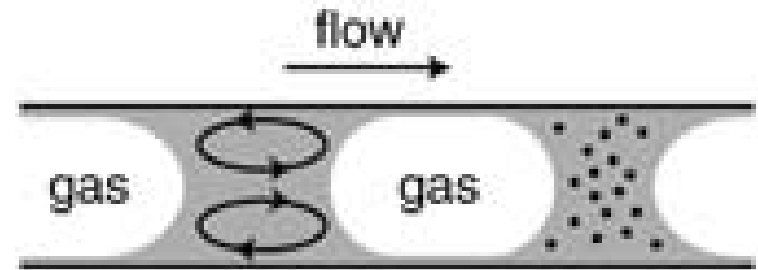
Segmented flow: gas-liquid

Gas divides liquid into small batch reactors

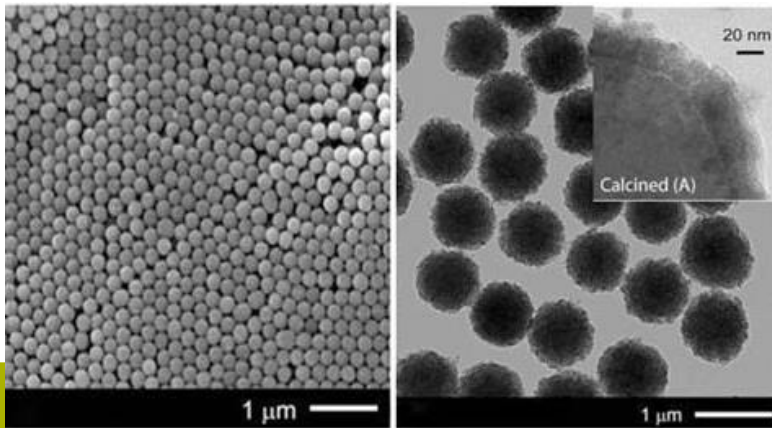
In case of (e.g. Silica or TiO_2)
particle growth:
particles close to wall grow longer



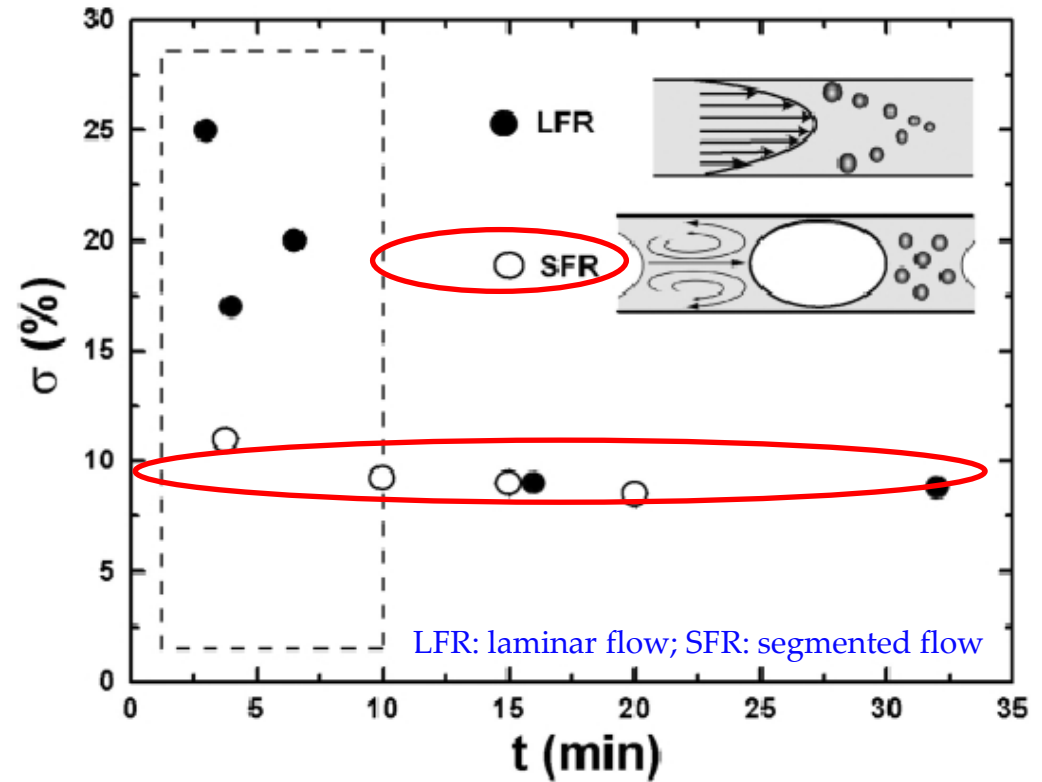
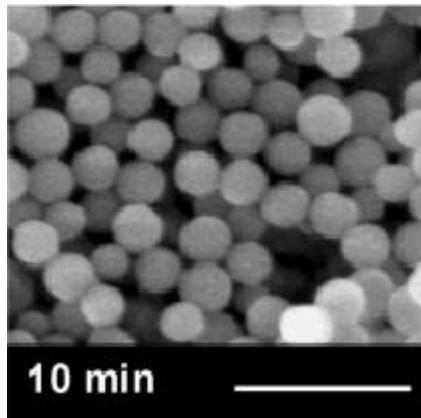
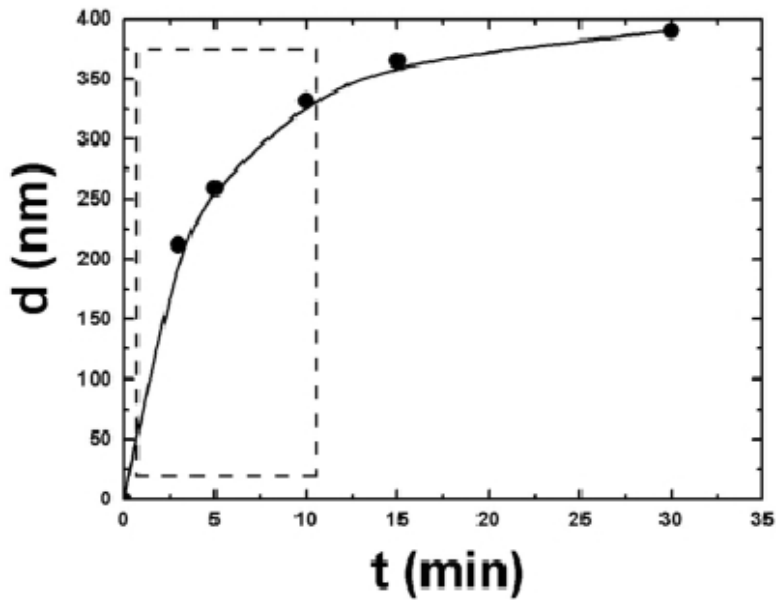
single-phase



segmented



Segmented flow: gas-liquid



Silica nanoparticles. Scalebar 1 μm

In-line demixing

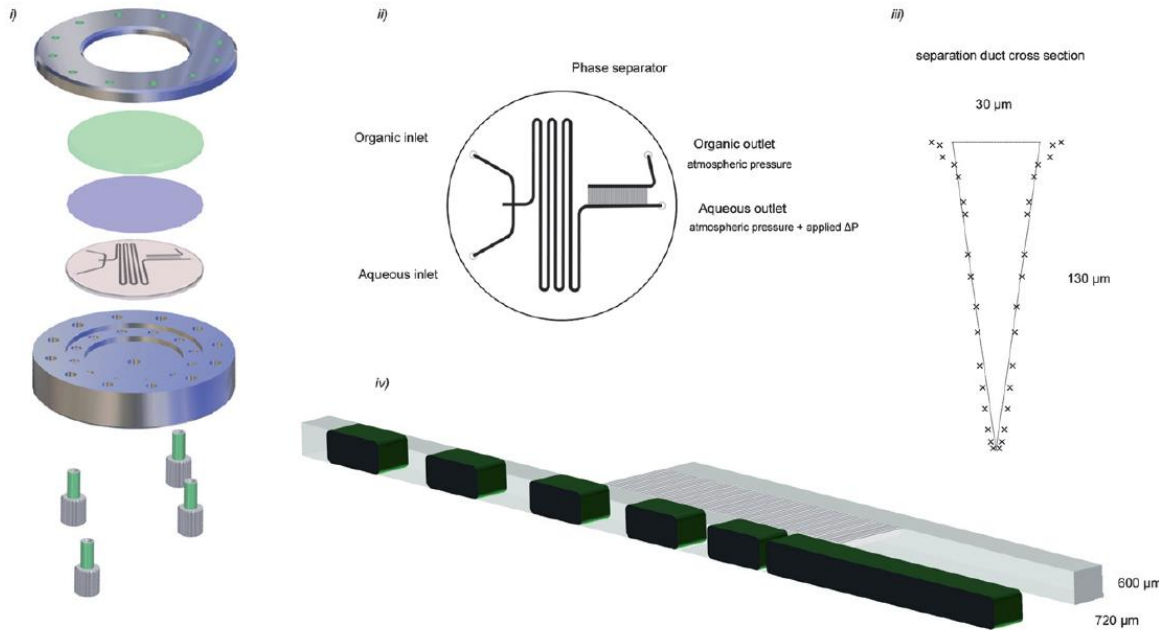


Fig. 2 Series of schematic diagrams illustrating (i) device construction. (ii) Microfluidic channel layout, including aqueous and organic inlets, T-junction for generation of segmented flow, phase separator region of the device consisting of a series of 140 parallel narrow side channels branching from the main fluidic duct leading to a designated organic outlet, with the main fluidic duct continuing to the designated aqueous outlet. (iii) Cross-sectional Gaussian profile of a single laser machined separation duct as measured by serial z-axis optical microscopy and the approximated triangular geometry used for modelling calculations. (iv) Cartoon illustration of the separator in operation, the organic phase (light) wets the PTFE channel walls and exits through the separation ducts, driven by the applied pressure differential between the two channel outlets. The non-wetting, aqueous fluid segments (dark) do not enter the narrow separation ducts but continue to flow in the main fluidic channel, coalescing into one continuous stream as the organic phase exits the channel.

720 μm wide, 600 μm deep

140 Side channels at phase separator: 36 μm wide, 130 μm deep

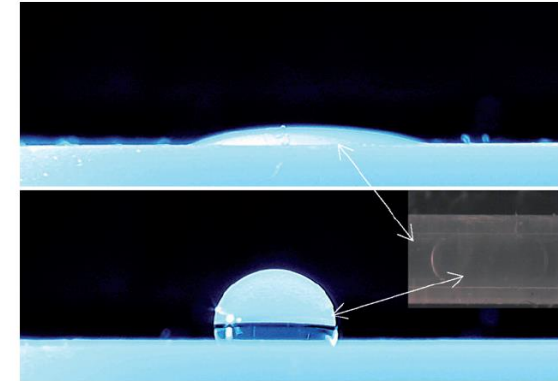
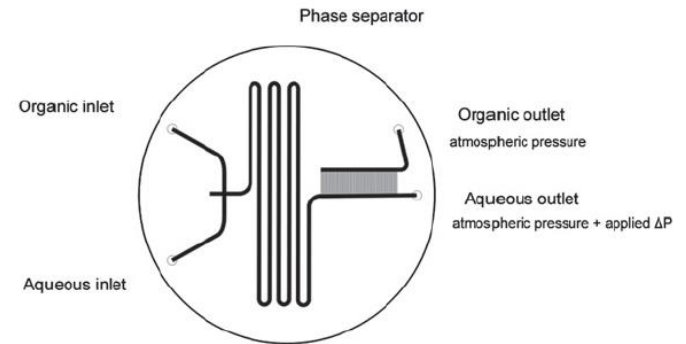


Fig. 3 PTFE wettability by chloroform (upper image) and water (lower image), drop volume 10 μl . Co-elution of the two liquids into a PTFE channel results in a segmented flow regime with chloroform wetting the channel walls as the continuous phase and water the disperse, droplet phase (inset image).

100 % efficiency separation

Non-coloured organic phase (chloroform) is wetting the teflon and flows in the narrow channels

Segmented flow: liquid-liquid



Laser machined PTFE
(polyfluoroethylene)

720 μm wide, 600 μm deep

140 Side channels at phase separator:

36 μm wide, 130 μm deep

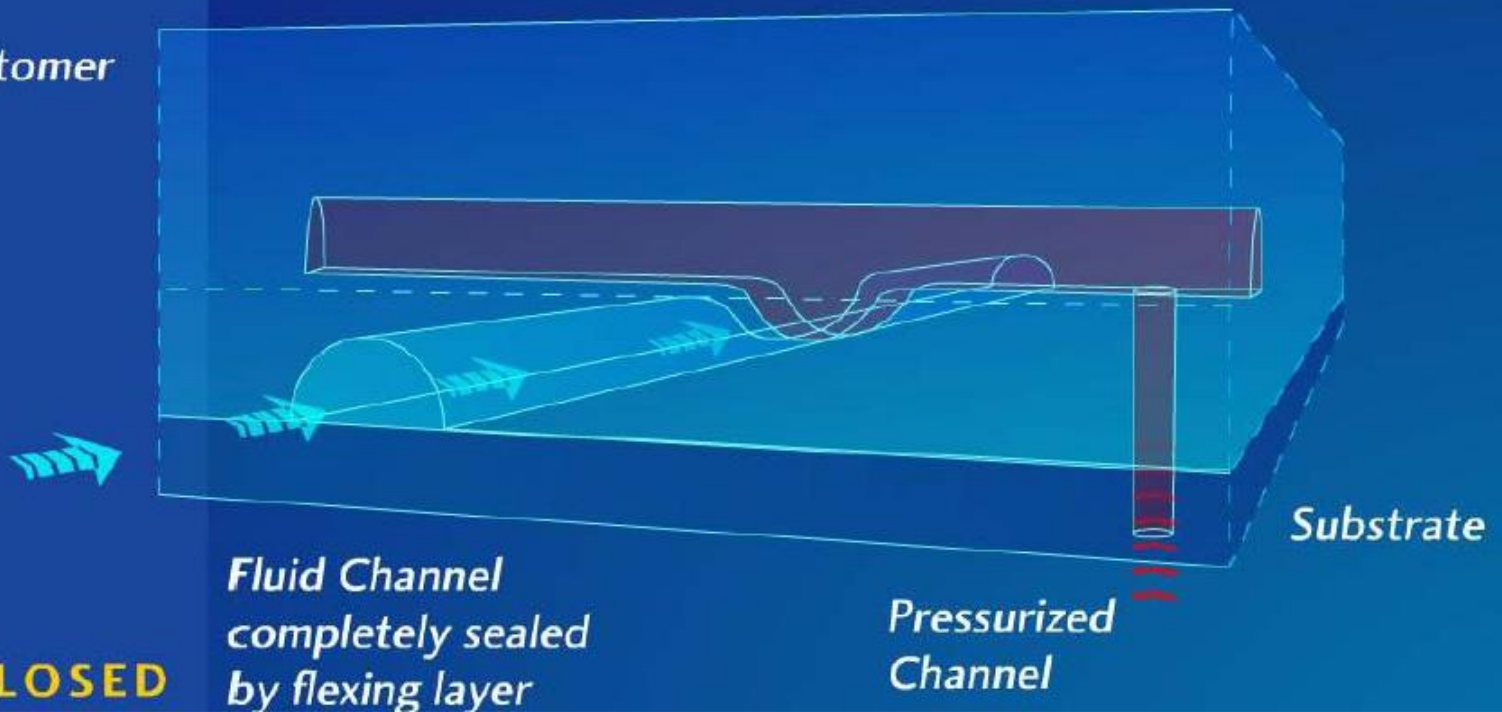
$\lambda=780\text{ nm}$, 0.55 W,

Machining speed: 50 mm/min

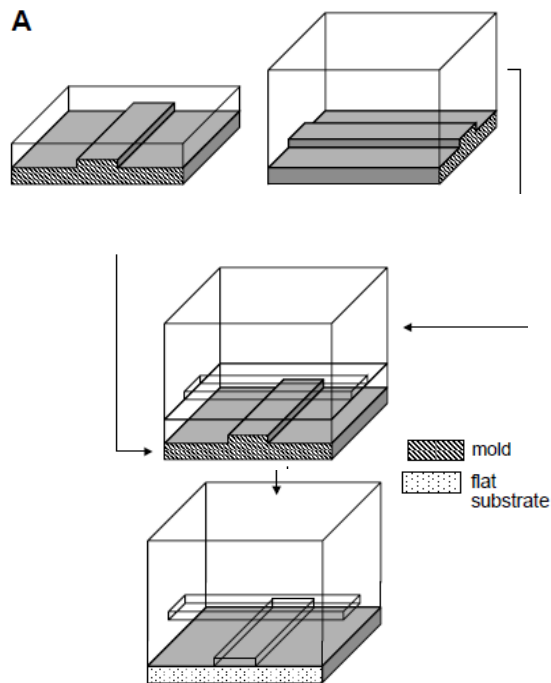
Valving

Air pressure is applied to the channel in the control (top) layer from an external source. This pressure causes the thin membrane between the layers to deflect into the fluid (bottom) channel, pinching off the flow of fluids.

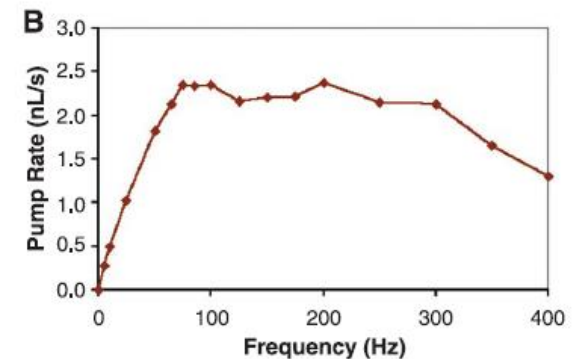
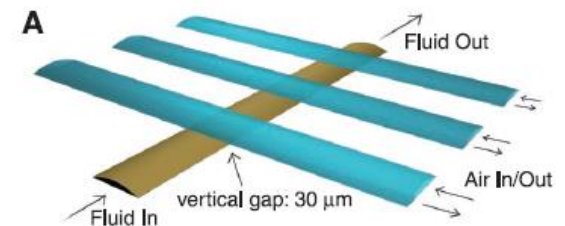
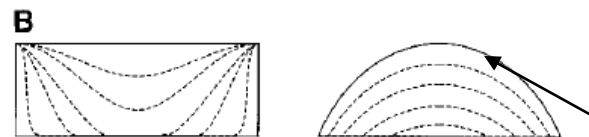
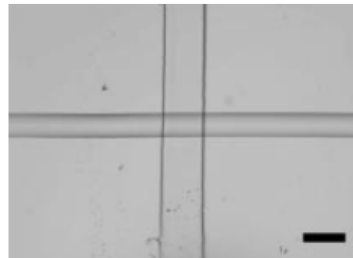
Elastomer



Valving/pumping



PDMS to PDMS
 Air actuated
 Membrane of 30 μm
 10 μm deep channel



Valves sequentially on-off:
 pumping

Complete sealing!
 (Only up to a few bar)

Multiple contents - screening



Emulsion polymerization

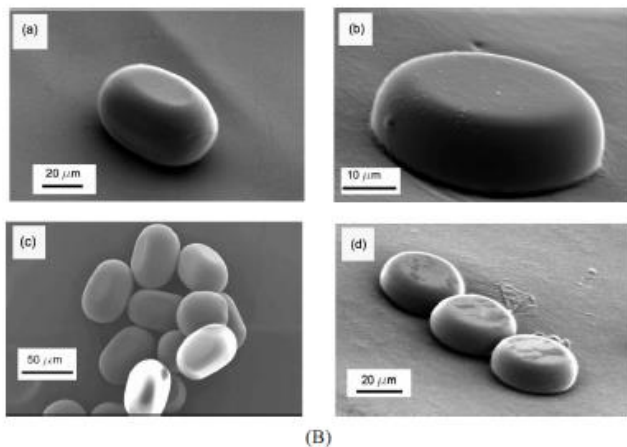
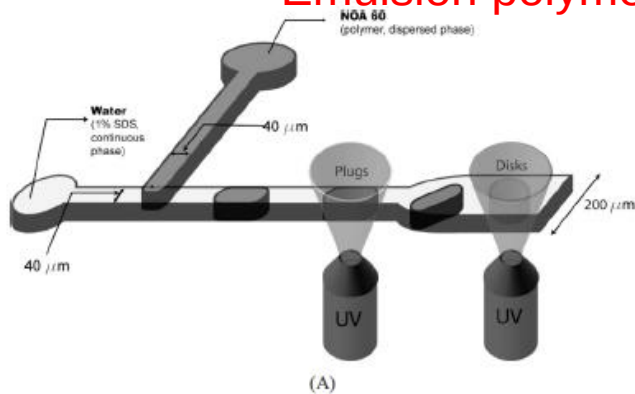
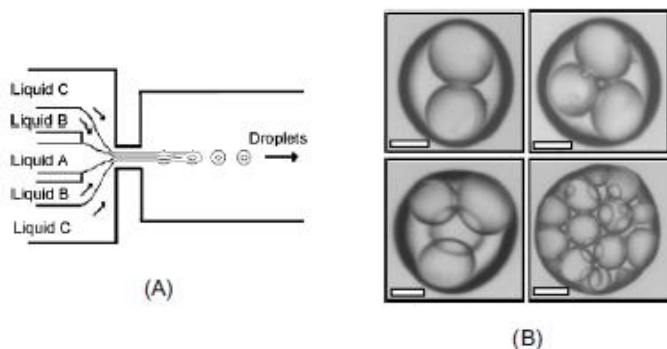


Figure 5. (A) Schematic depicting the T-junction microchannel device for production of non-spherical polymer particles. (B) SEM images of plug-shaped particles (a, c) and disk-like particles (b, d) (from ref. [10]).

Complex emulsion particles



Lock release

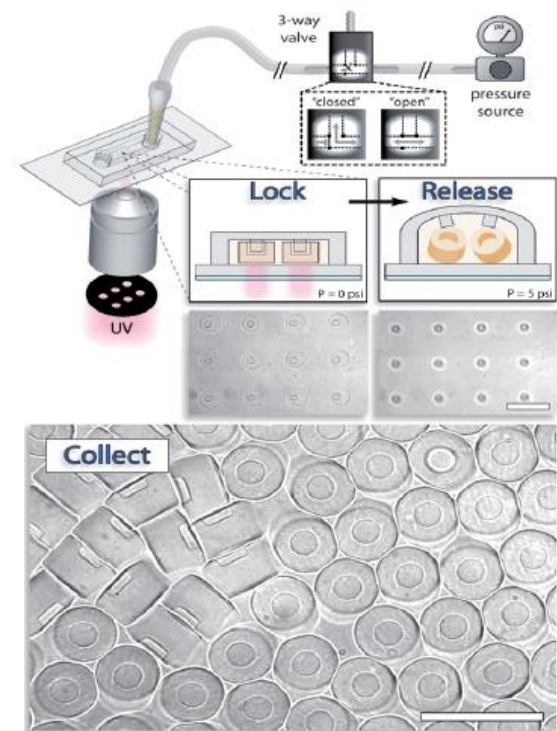
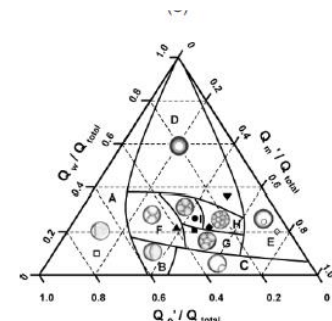
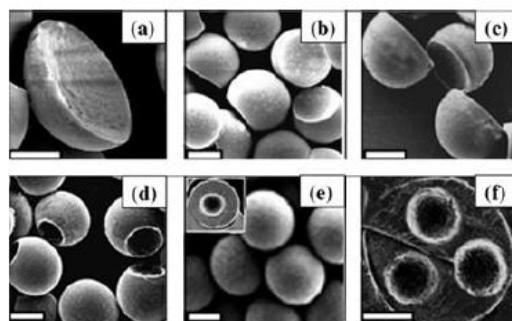
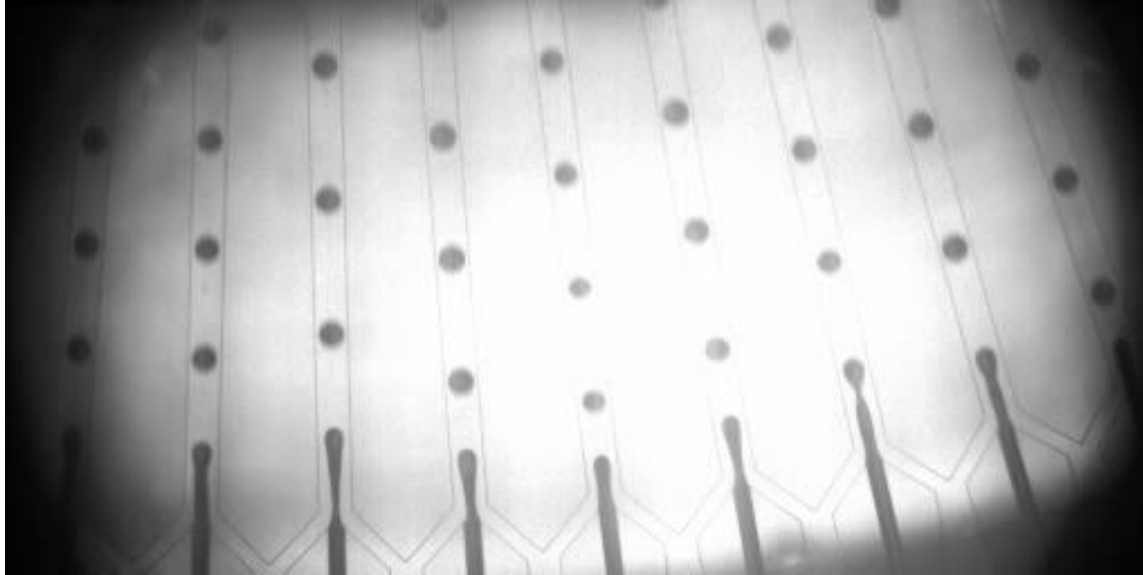


Fig. 1 Process of lock release lithography. First, structures are polymerized by shining bursts of UV light through a transparency mask and a microscope objective. The particles with shapes determined by the mask and channel topography, are "locked" by relief structures in the channel topographies. Particles are "released" with channel deflection after a relatively high pressure (~ 5 psi) is applied to initiate flow. Shown is a differential interference contrast (DIC) image of a collection of 3D particles with micro-cavity in the channel reservoir. Scale bars are 100 μm .



Parallelization



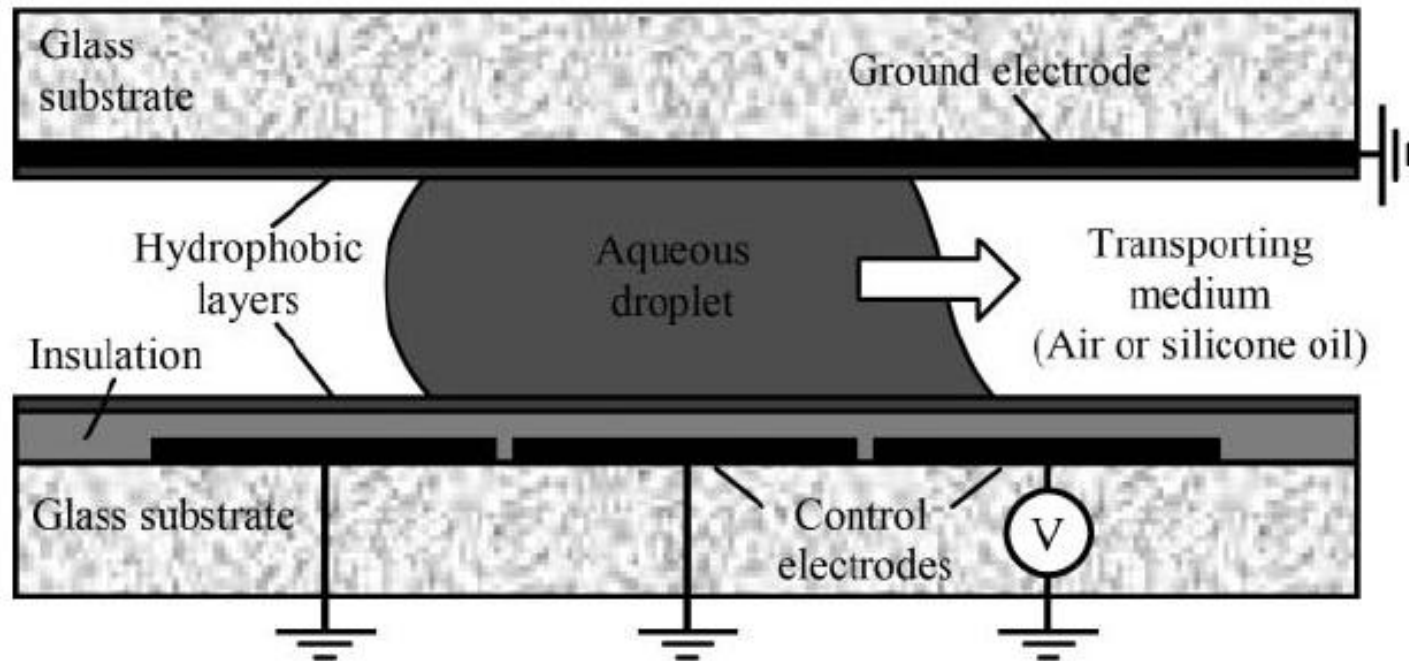
Glass chips (fusion bonded)
depth 100 μm
Width 100 & 200 μm

to be disp. Phase: 1,6 hexanediol diacrylate
with photoinitiator

Aqueous phase: polyvinylalcohol (2%) in H_2O

In this study, we report the mass production of monodisperse emulsion droplets and particles using microfluidic large-scale integration on a chip. The production module comprises a glass microfluidic chip with planar microfabricated 16–256 droplet-formation units (DFUs) and a palm-sized stainless steel holder having several layers for supplying liquids into the inlets of the mounted chip. By using a module having 128 cross-junctions (*i.e.*, 256 DFUs) arranged circularly on a 4 cm $\times$ 4 cm chip, we could produce droplets of photopolymerizable acrylate monomer at a throughput of 320.0 mL h^{-1} . The product was monodisperse, having a mean diameter of 96.4 μm , with a coefficient of variation (CV) of 1.3%. Subsequent UV polymerization off the module yielded monodisperse acrylic microspheres at a throughput of $\sim 0.3 \text{ kg h}^{-1}$.

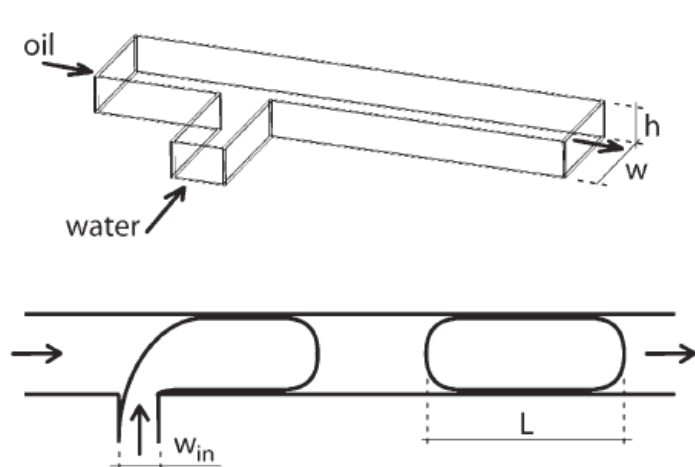
Contact angle manipulation



Digital μ Fluidics



Emulsion approach: other opportunity for microreactor format



$$L/w = 1 + \alpha Q_{in}/Q_{out}$$

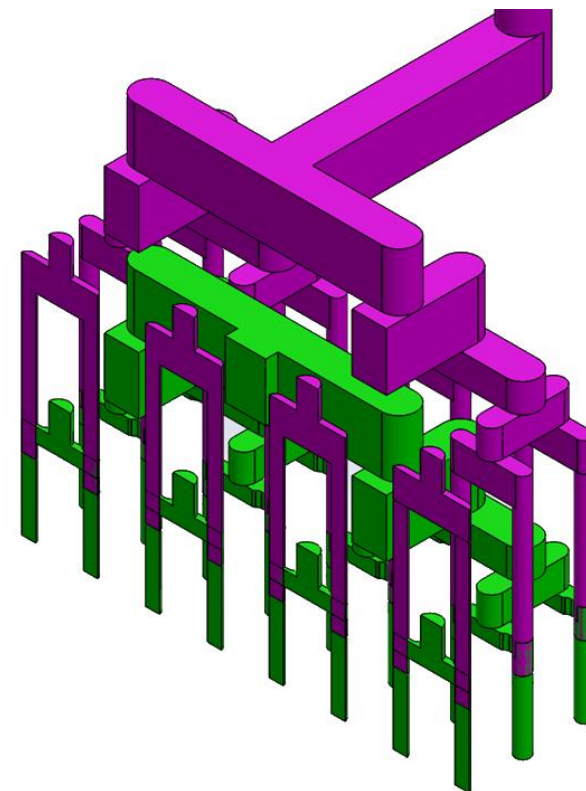
CV: <7% vs. 25-80 % (smx and batch)

Formation of droplets and bubbles in a microfluidic T-junction—scal and mechanism of break-up†

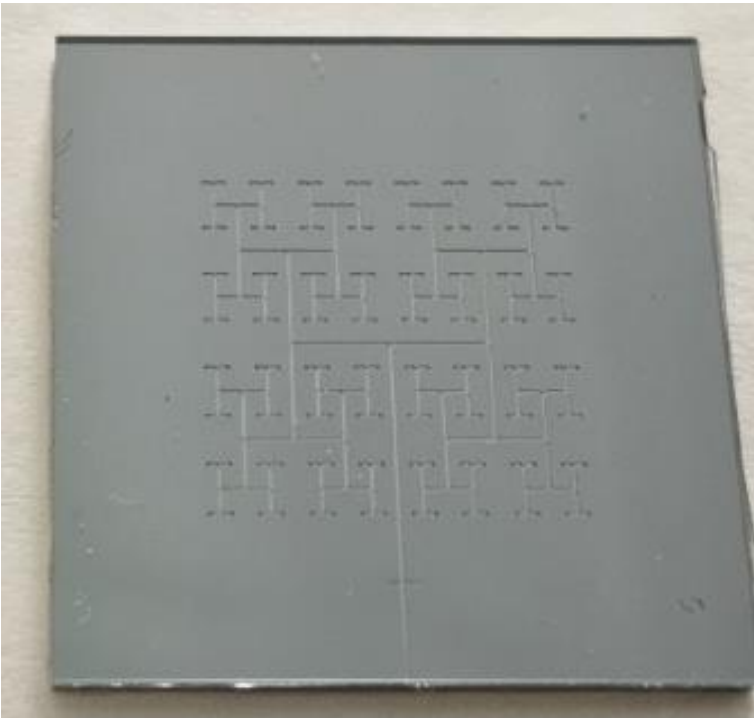
Piotr Garstecki,^{*ab} Michael J. Fuerstman,^a Howard A. Stone^c and George M. Whitesides^{*a}

Received 29th July 2005, Accepted 5th January 2006

Lab Chip, 2006, 6, 437–446 | 437

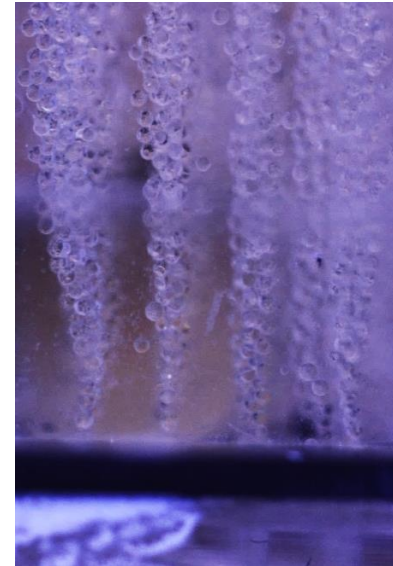
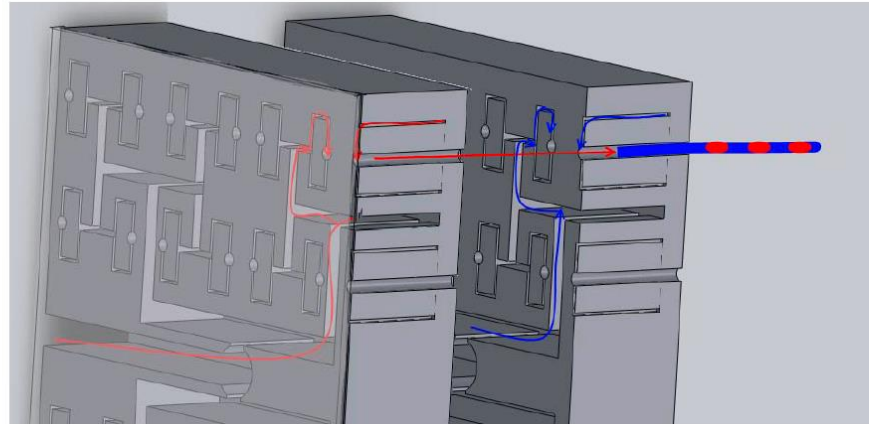


Industrial scale emulsification

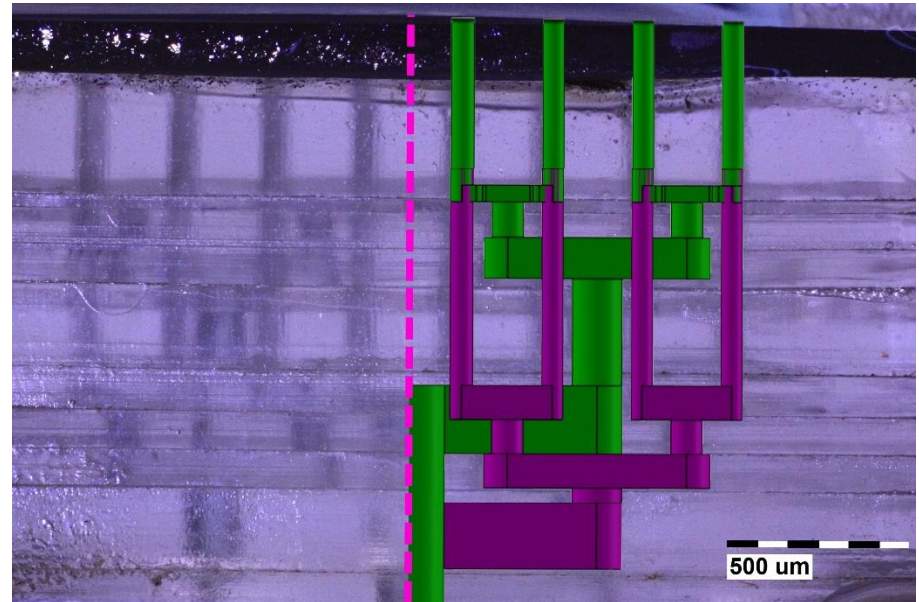
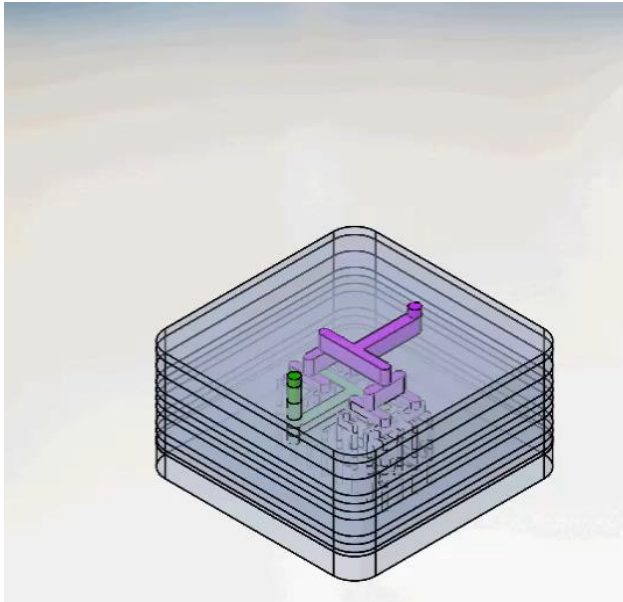


400 μm hexane droplets in water
+ SDS (CV ~10 %)
5 bar: 10 ml/min (64 nozzles)

Patent pending



Chip assembly



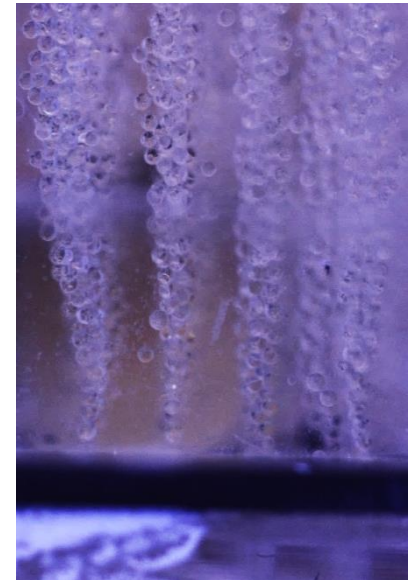
Several layers (11) are stacked and thermally bonded @ 155 C for 50 min under 5 kg weight (PMMA)

Reversible procedure with fluoroelastomer

On-chip characterization

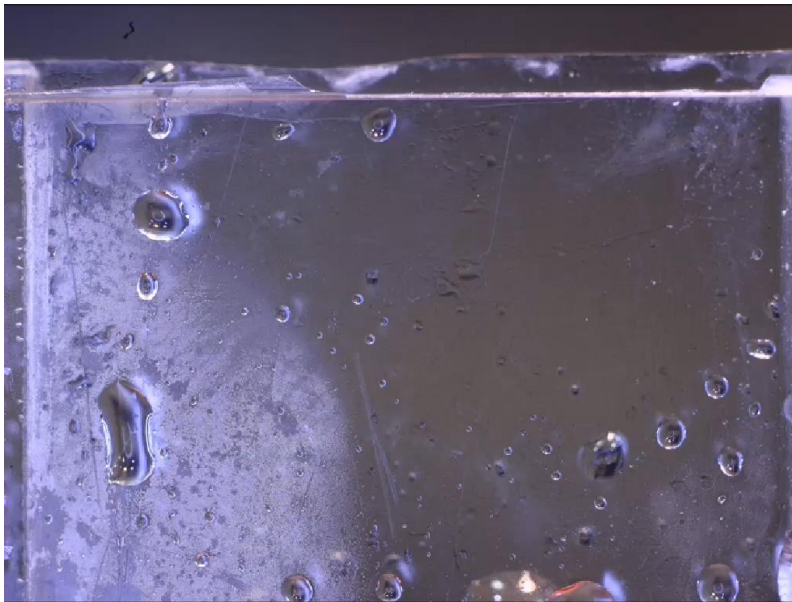
0. 4 mm droplets
(CV ~10 %)

Hexane droplets in water+SDS
5 bar: 10 ml/min (64 nozzles)

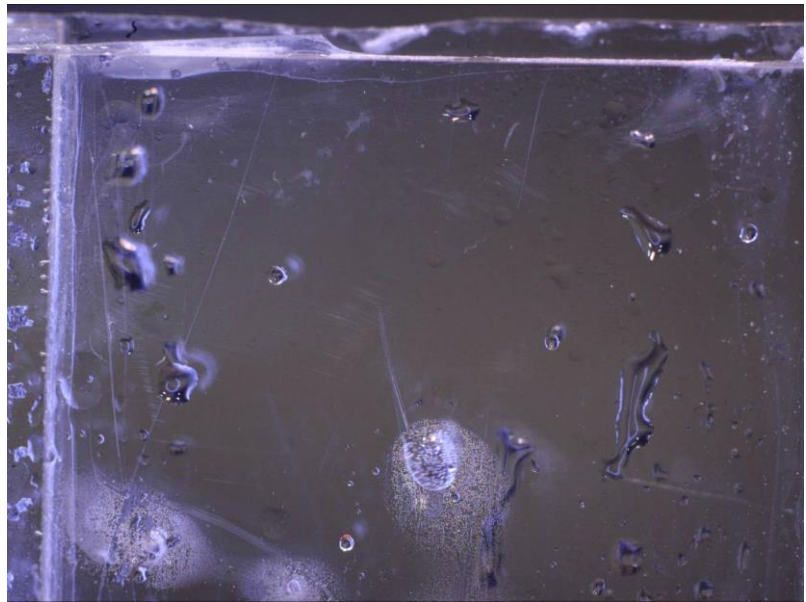


Enhanced phase separation

Multi-nozzle array (CV ~10 %)



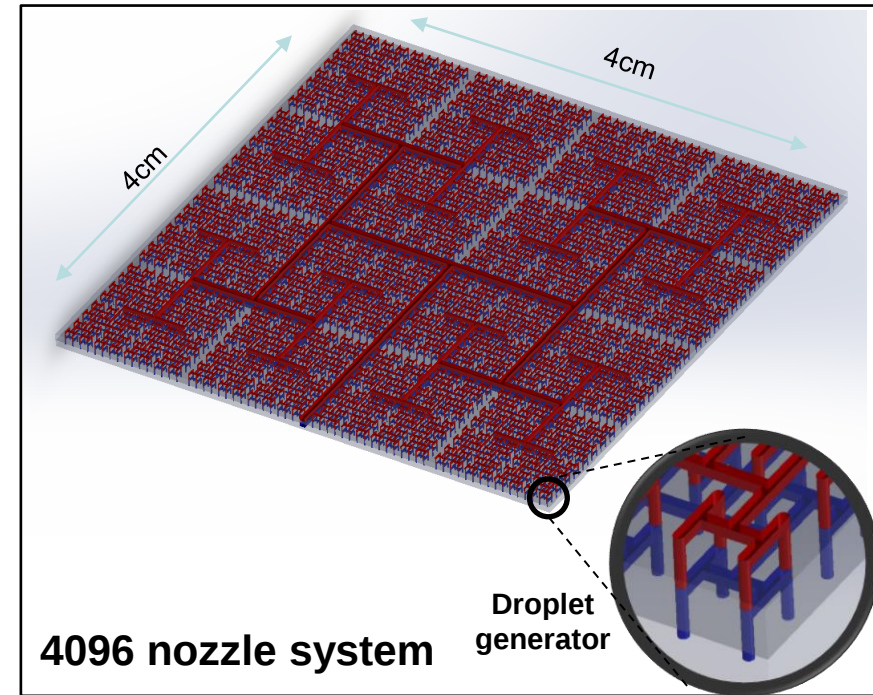
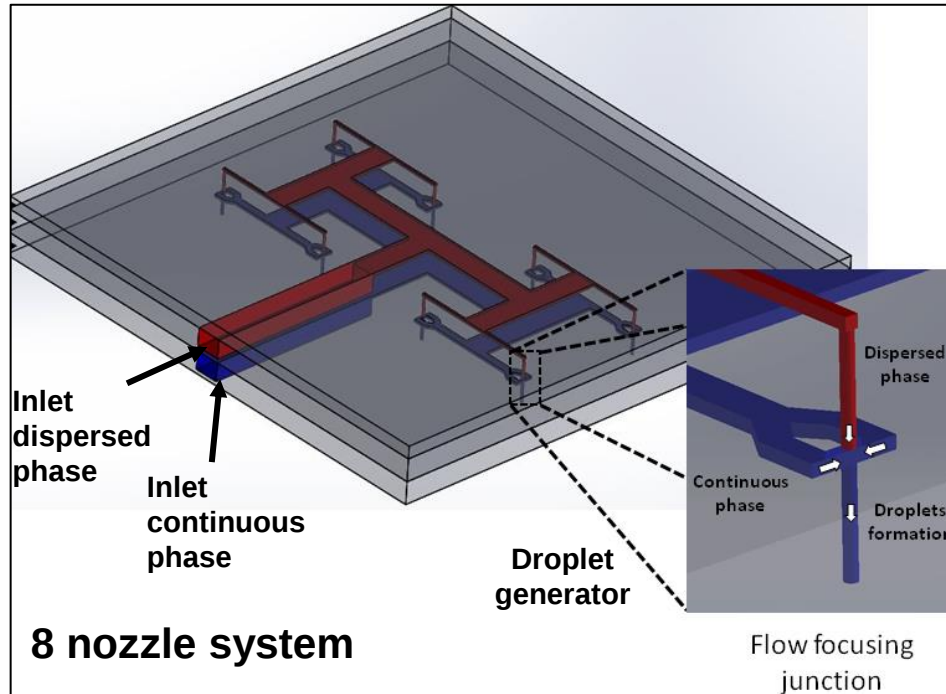
Mixer (CV ~ 35 %)



3D flow distribution

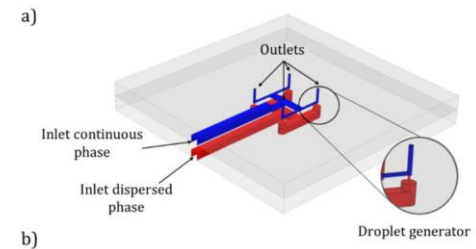
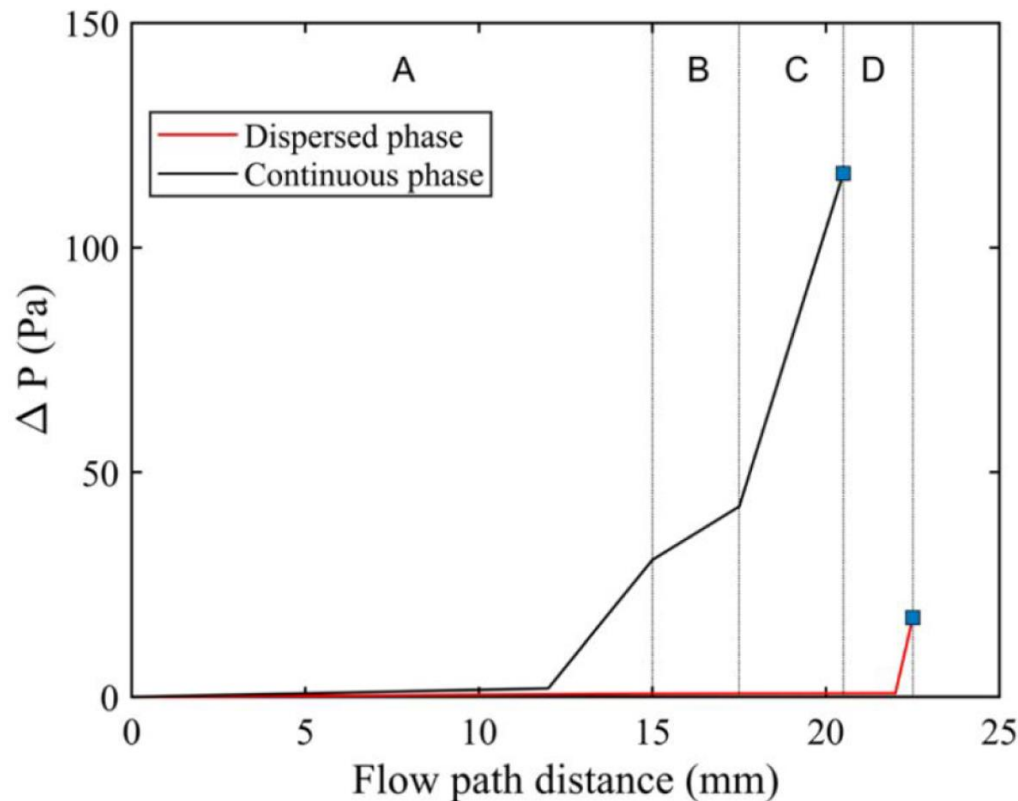
maximizing number of nozzles / surface

3D emulsifier:
microfluidic design for a high throughput
droplet production



Pressure drop at branches

A (first layer)....D (nozzle)



Nozzle diameter 150 μm
Channel depths: 200 μm
Width: 1 mm to 300 μm

5 ml/h/nozzle

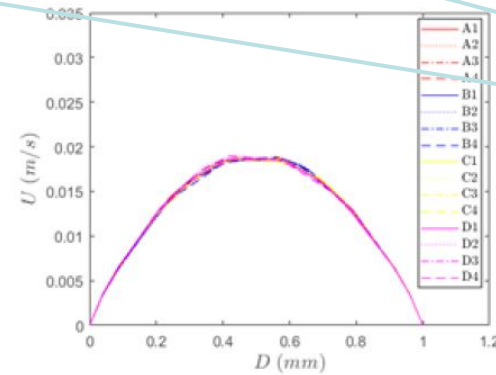
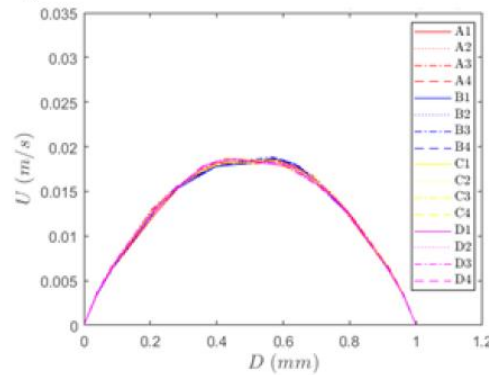
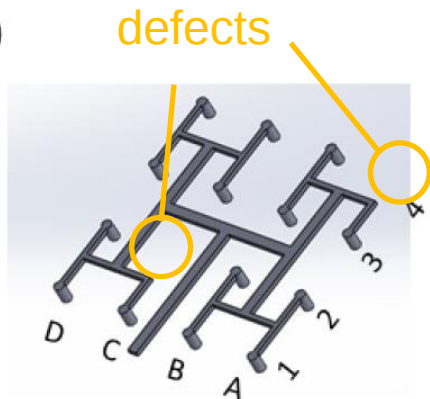
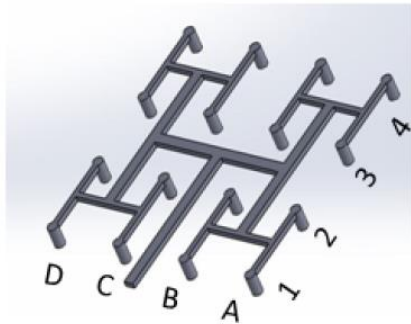
(Reducing) sensitivity to fouling

$h=500\text{ }\mu\text{m}$

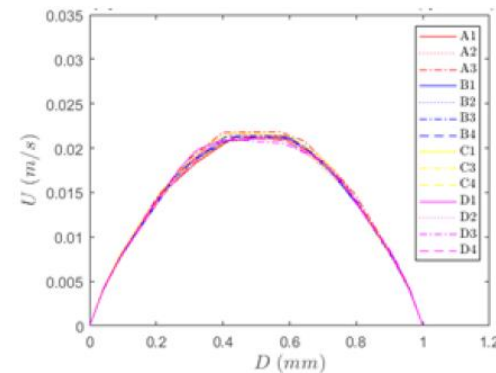
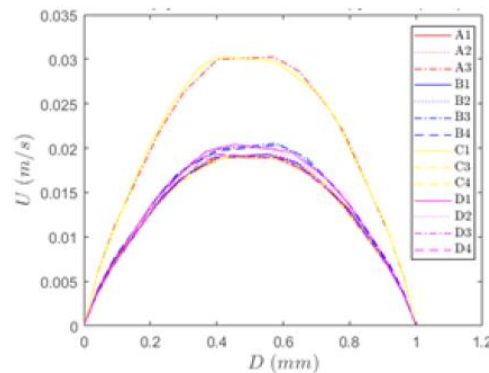
Channel depths

1 mm – 1 mm
- 1 mm – 0.5 mm
- 0.5 mm

1 mm – 1 mm -
1 mm – 0.5 mm
- 0.1 mm

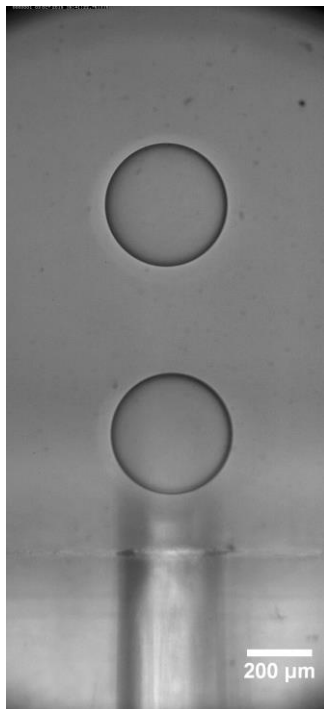


*Last channel
before
through-hole*

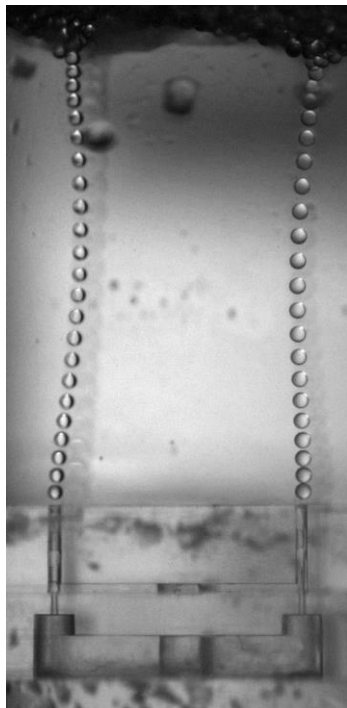


Throughput considerations

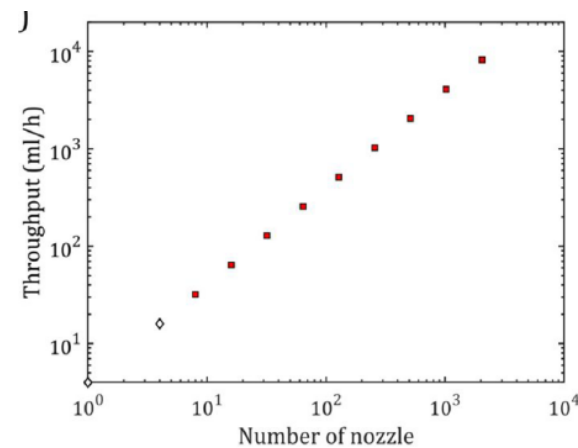
PMMA chips



Outlet



Overview



100 μm channels

2048
nozzles on 1
 cm^2 :
8.2 l/h

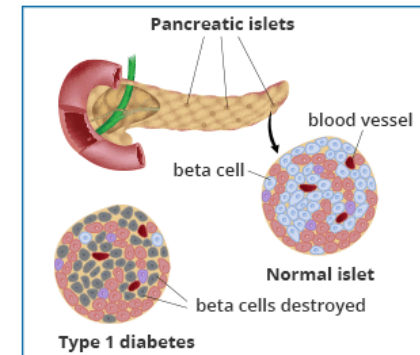
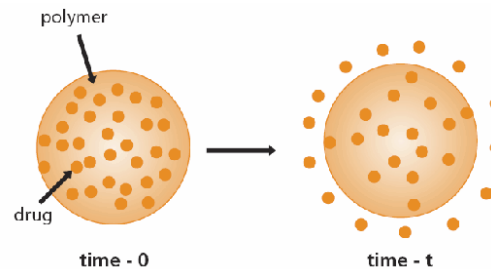
- Biodegradable polymer

- Drug release

- Cancer treatment
- ...
- **Cell therapy for diabetes**

- Basic Mechanism

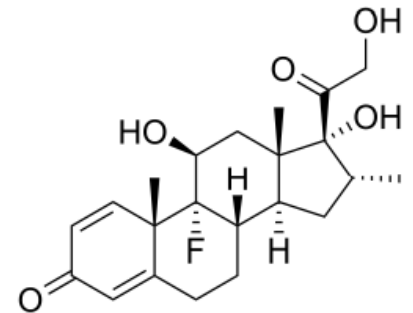
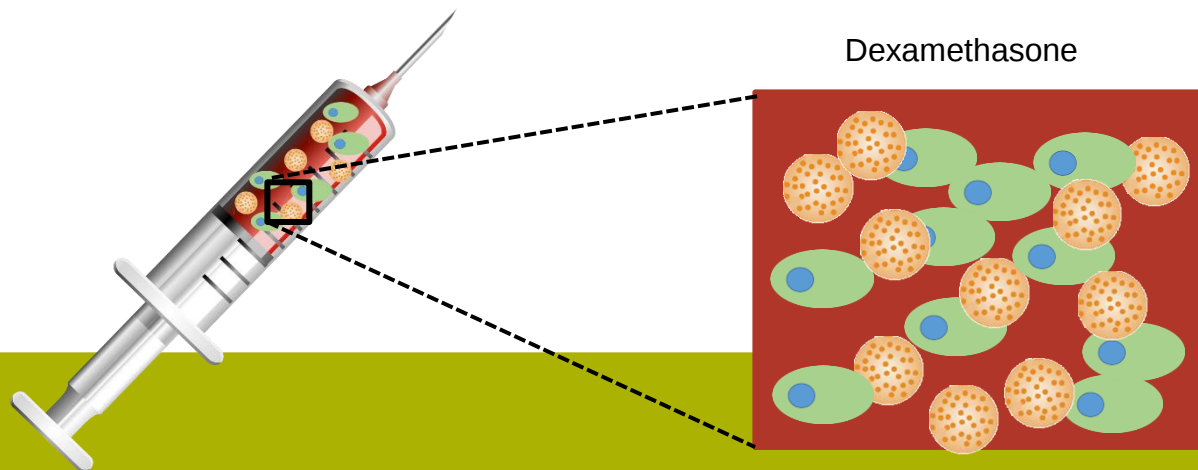
- Slow degradation of the polymer, releasing the drug into the environment



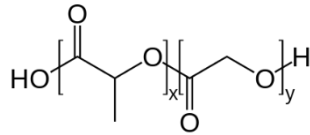
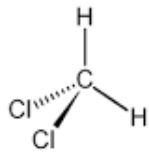
PLGA: motivation

Collaboration with Prof. Karine Hellemans (Diabetes Research Center, Brussels)

- Motivation
 - Inject alongside implant (β -cells)
 - Diameter: 10-50 μm
 - Dexamethasone loaded particles
 - Prevent inflammation
 - Induce β -cell proliferation

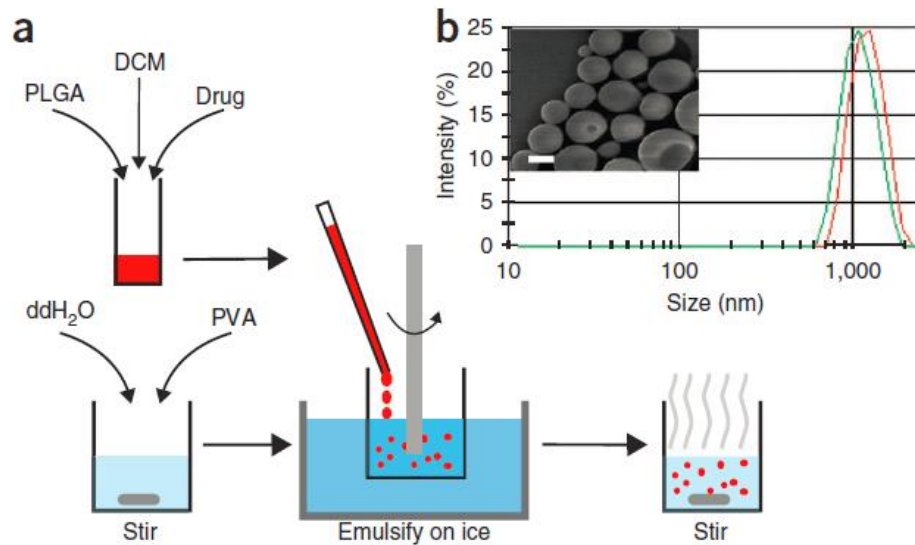


PLGA particles – cell therapy

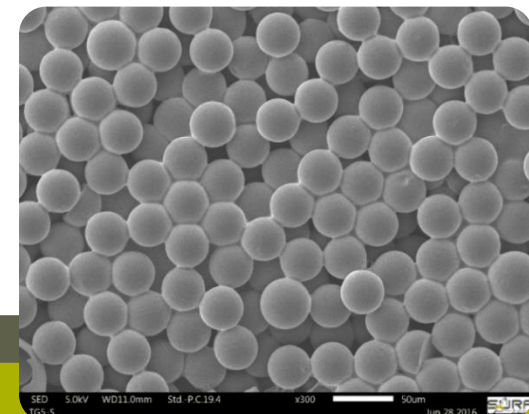
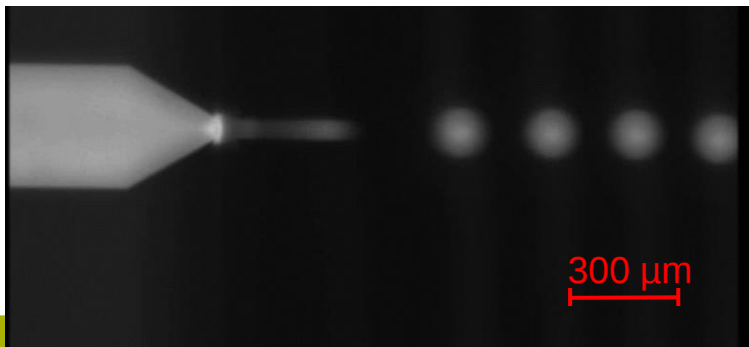


PLGA: poly(lactic-co-glycolic acid)

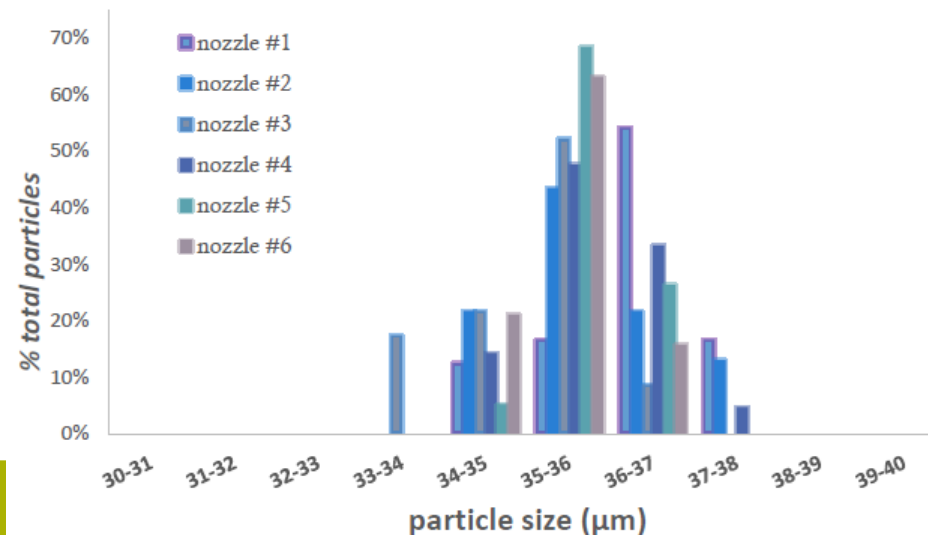
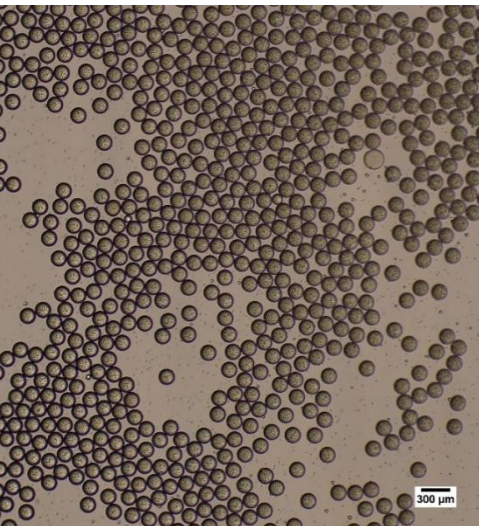
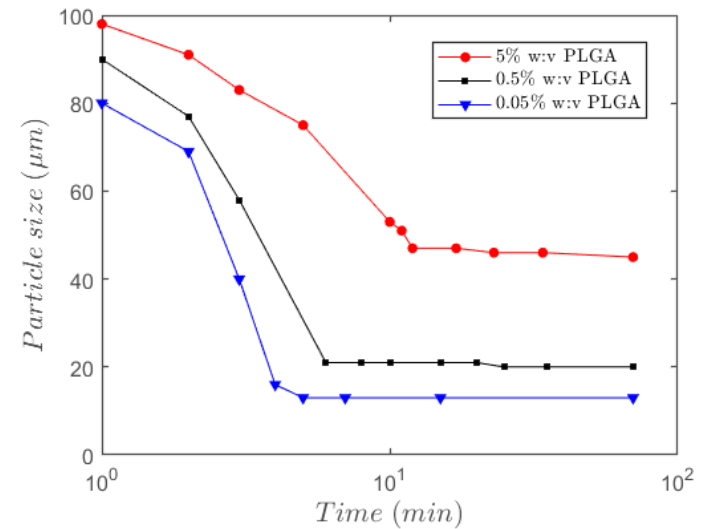
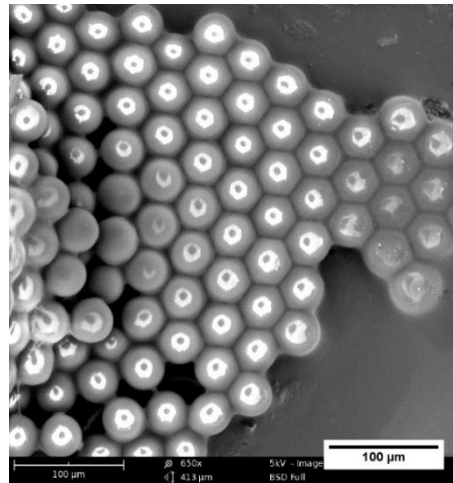
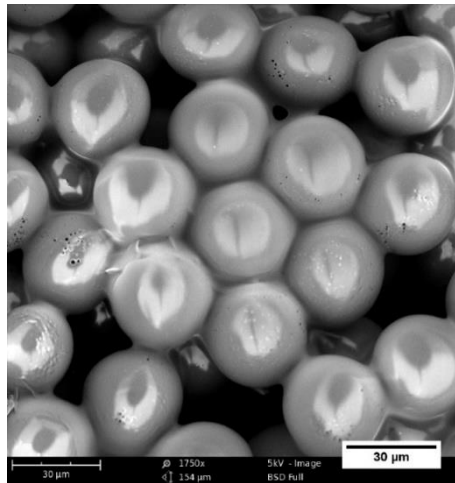
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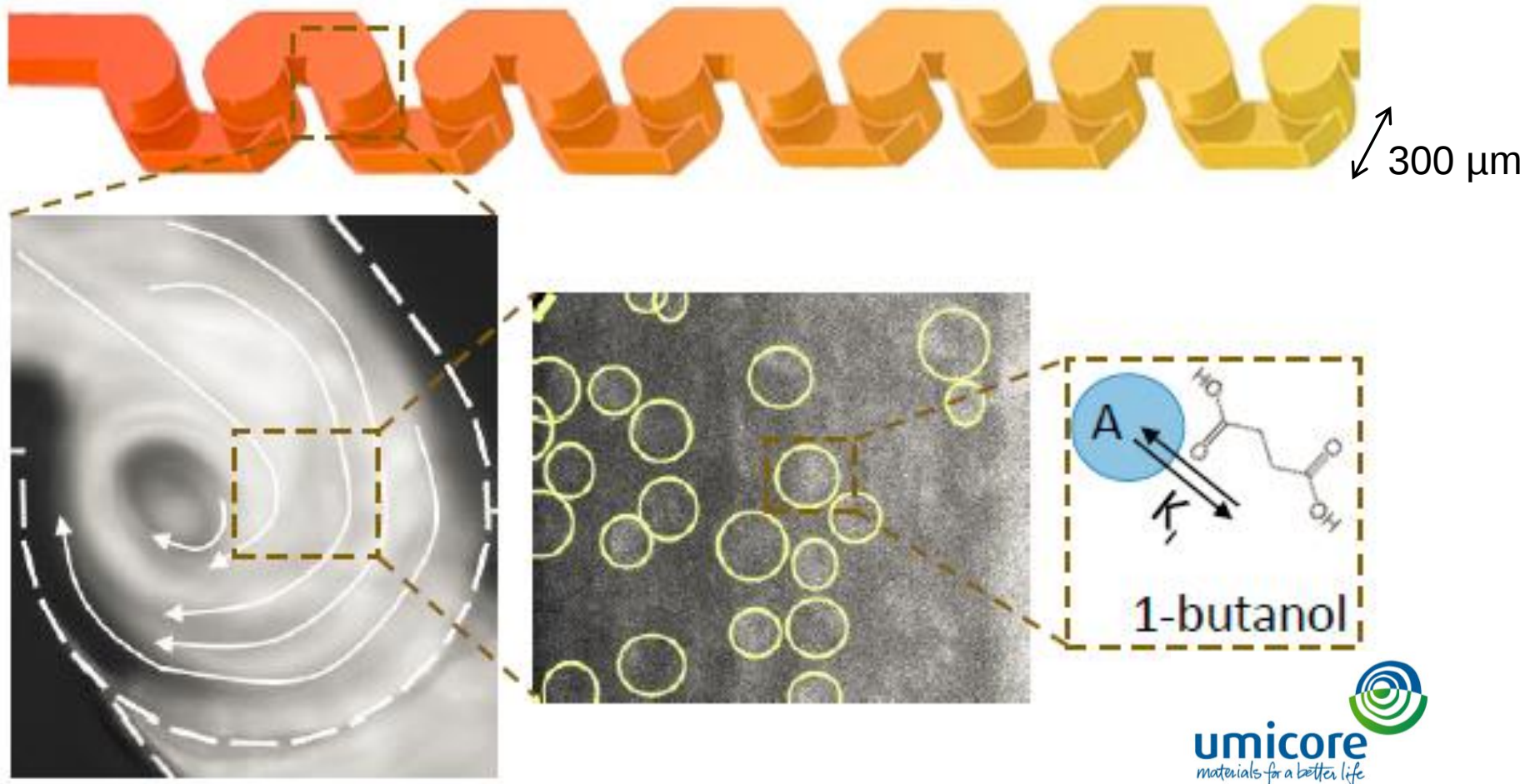
Type 1 diabetes: β cell therapy
Promotion of favorable factors



PLGA particles, loaded with dexamethasone



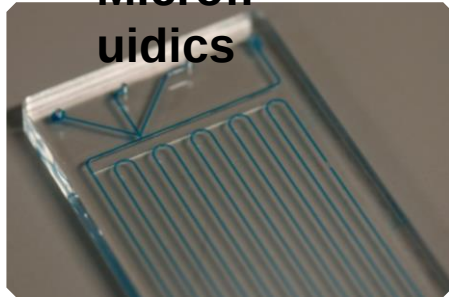
Vortex contact – geometrical approach



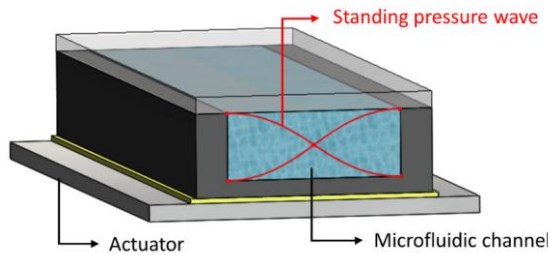
ACOUSTICS

Acoustofluidics

Microfluidics



Acoustics



Lab on a Chip tutorial series on
acoustofluidics: Acoustofluidics—exploiting
ultrasonic standing wave forces and acoustic
streaming in microfluidic systems for cell and
particle manipulation

Henrik Bruus,^a Jurg Dual,^b Jeremy Hawkes,^c Martyn Hill,^d Thomas Laurell,^e Johan Nilsson,^e Stefan Radel,^f
Satwinder Sadhal^g and Martin Wiklund^h

DOI: 10.1039/c1lc99058g

Acoustofluidics = ultrasound-based manipulations in microfluidic devices

Acoustofluidics

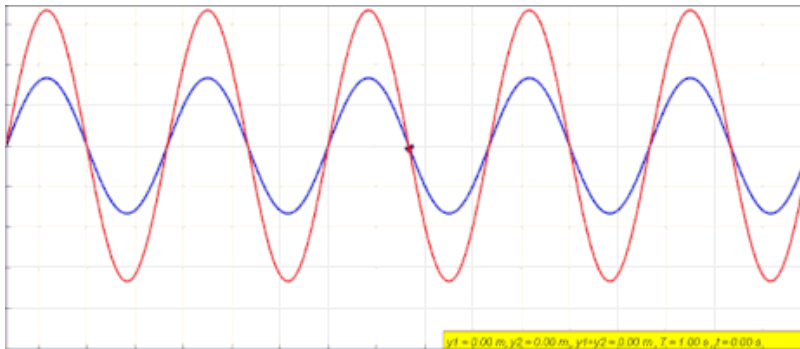
- Operates in the MHz range $\rightarrow \lambda < 1$ mm
- Maximum energy transfer at resonance frequency $\rightarrow$ generate a standing wave
- Criterion for a standing wave in micro-cavity:

$$\text{Channel width} = n * \frac{\lambda}{2}$$
$$\text{wavelength } \lambda = c/f$$

c: Speed of sound [m/s]

f: Frequency [Hz]

λ : Wavelength [m]

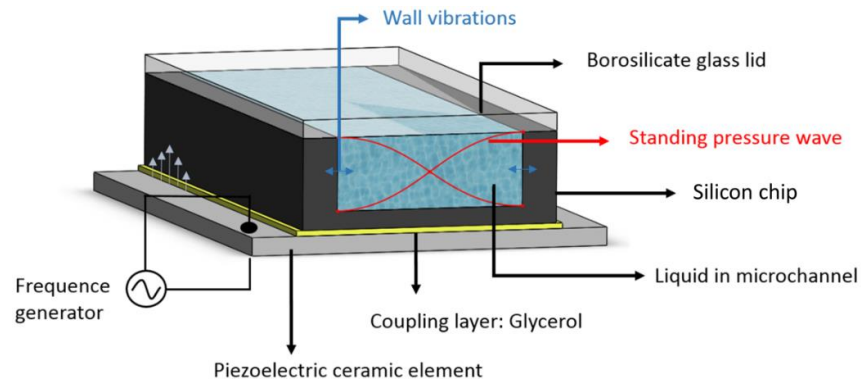


$$f(x, t) = A * e^{i(kx \pm \omega t)}$$

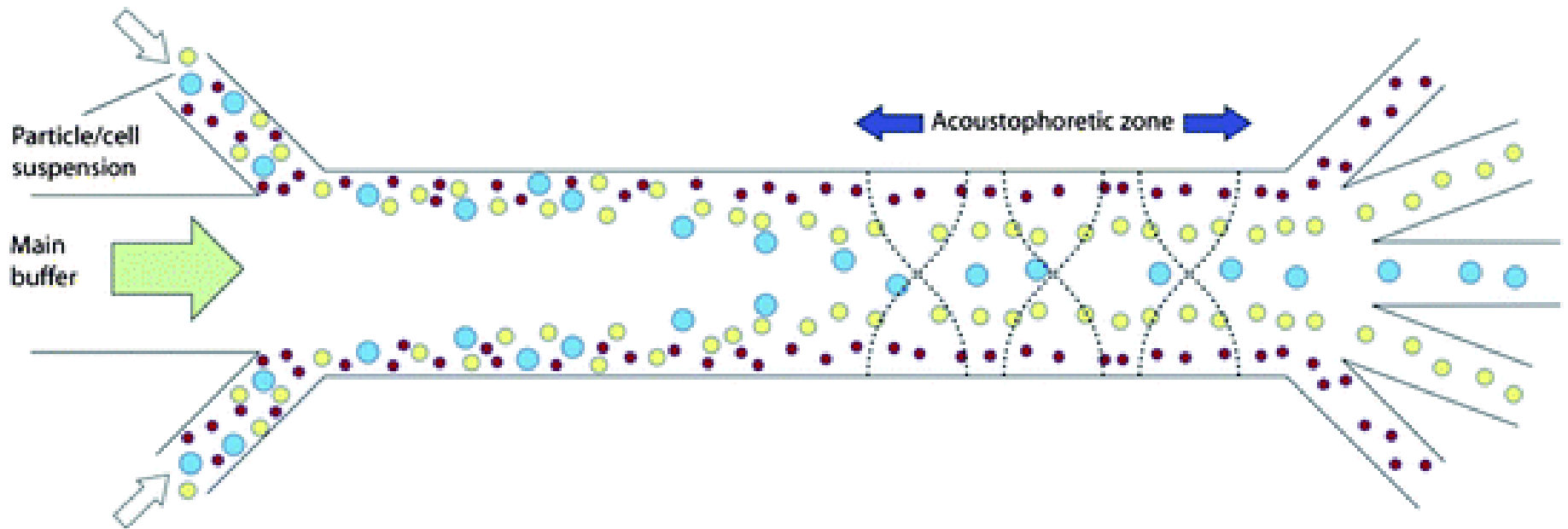
Acoustofluidics

- **Bulk acoustic waves (BAW)**

- Whole device vibrates and standing wave is generated in “matched” direction
- Generated by piezoceramic element (PZT)
- Chip made of non-elastic material to ensure reflection of pressure wave (glass; silicon; metals; ...)
- Frequency: 1 - 10 MHz



Acoustophoresis of particles



A. Lenshof. Lab on a Chip,
2012

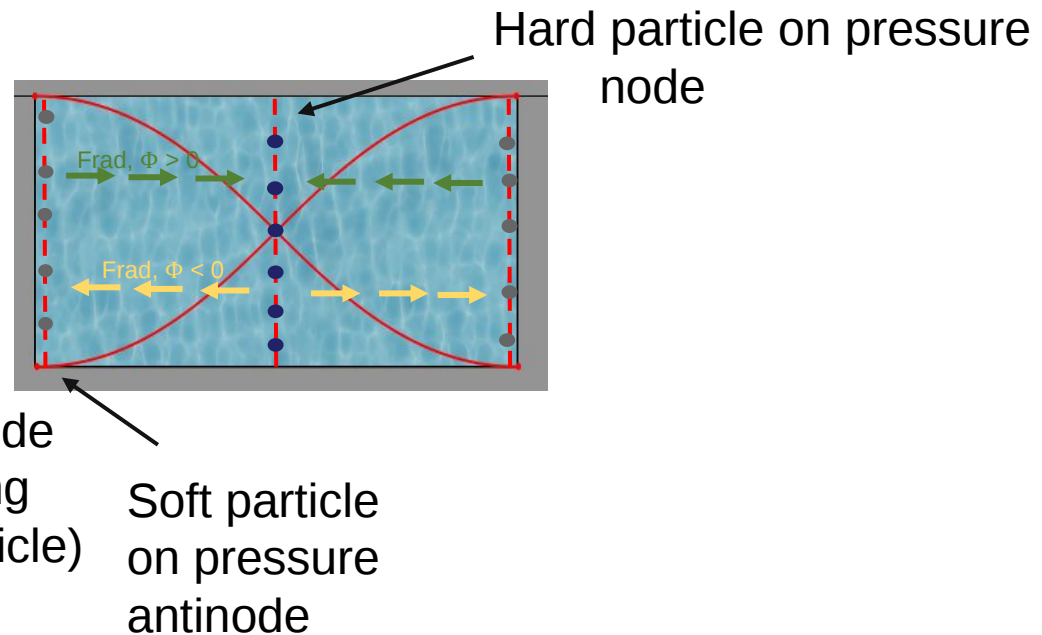
Acoustic manipulation of particles

Particles are affected by acoustic field:

- Radiation force: $F_{rad} = n4\pi \Phi a^3 \frac{E_{ac}}{\omega} \sin(n2\pi \frac{y}{\omega} + n\pi)$
- Stokes drag force: $F_{drag} = 6\pi\eta a (v_{liq} - v_{particle})$

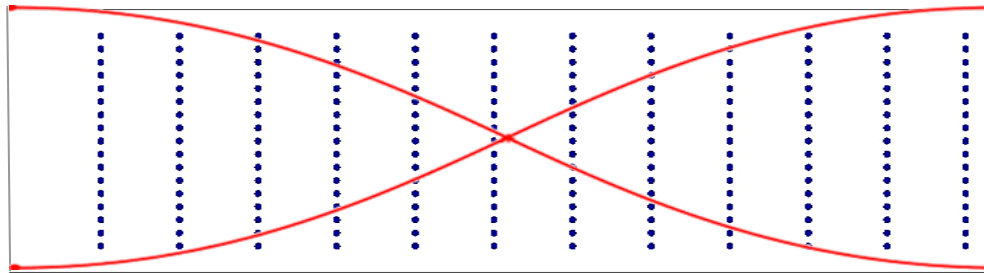
Particle diameter

- Small particles (<2 μm)
 - Mostly influenced by F_{drag}
 - Follow liquid vortices
- Large particles (>2 μm):
 - Affected by F_{rad}
 - Focus in pressure node or antinode depending on Φ . (Hard/Soft particle)

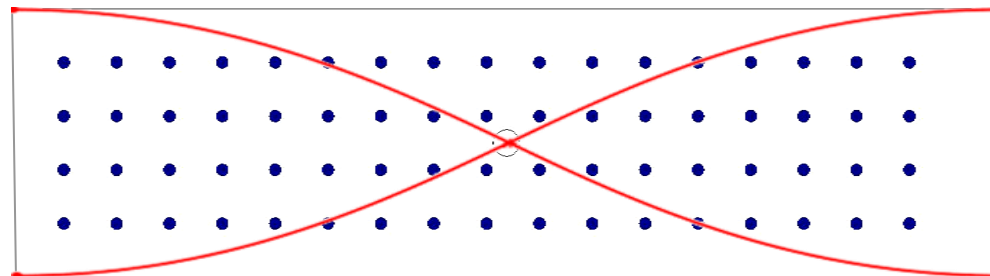


Acoustic manipulation of particles

Polystyrene particles diameter= 0.5 μm

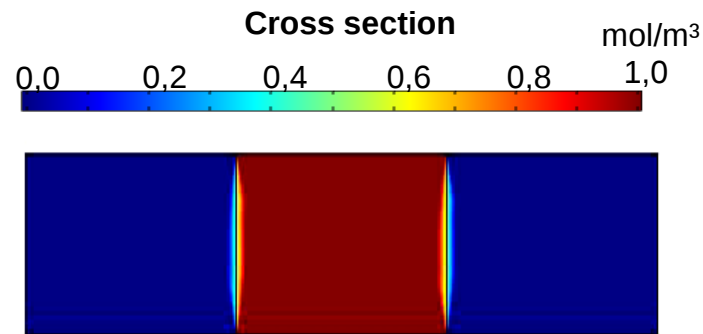


diameter= 5.0 μm



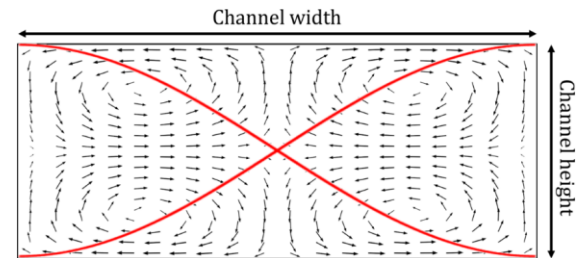
Comsol simulation, unpublished, μFlow group

Enhanced mixing with acoustics

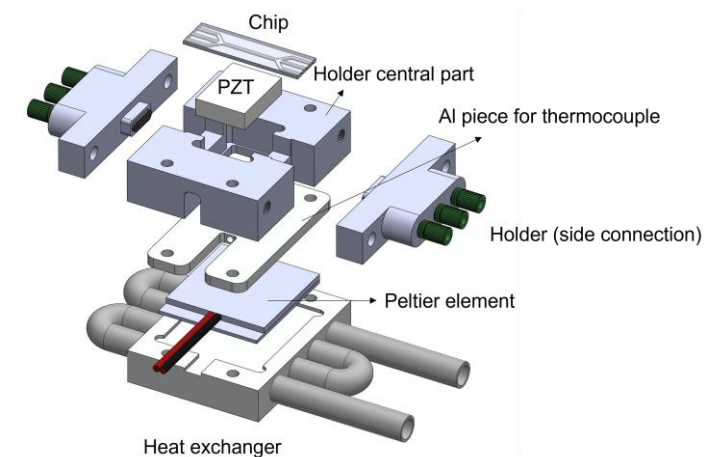
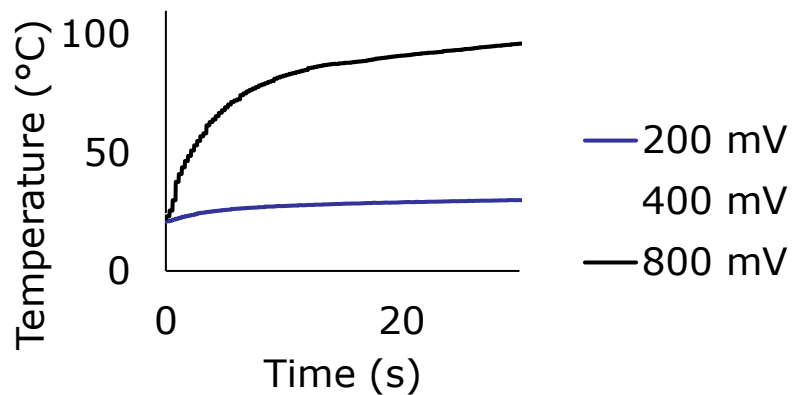


sub-s mixing
in a 375 μm channel

Gelin, P., Sukas, O., Hellemans, K., Maes, D., De Malsche, W. (2019),
Study on the mixing and migration behavior of micron-size particles in
acoustofluidics, Chemical Engineering Journal, 369, 370-375



Acoustics - heating considerations

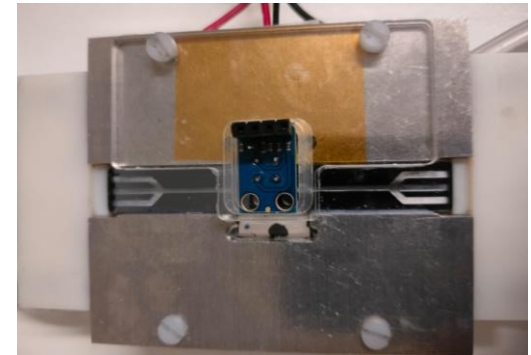
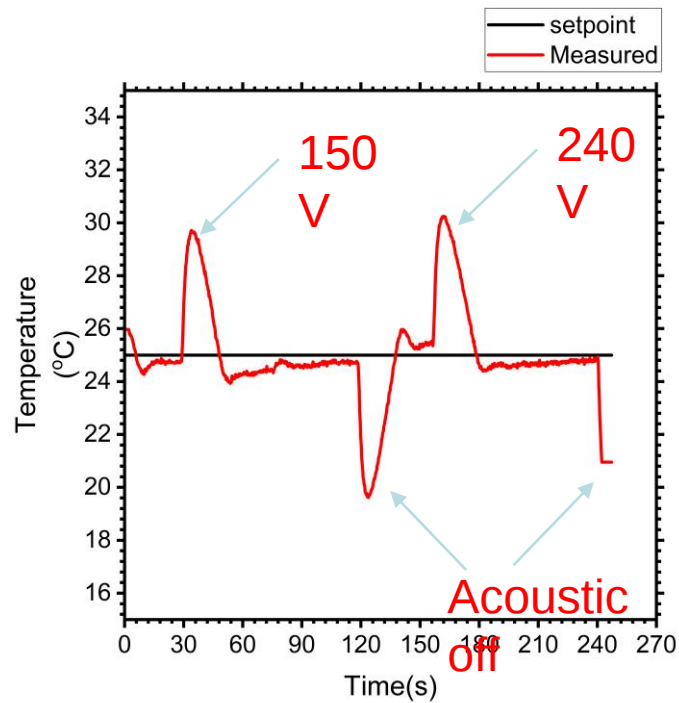


When actuated, the PZT generates heat depending on the voltage applied

-> interference with the primary source of waves.

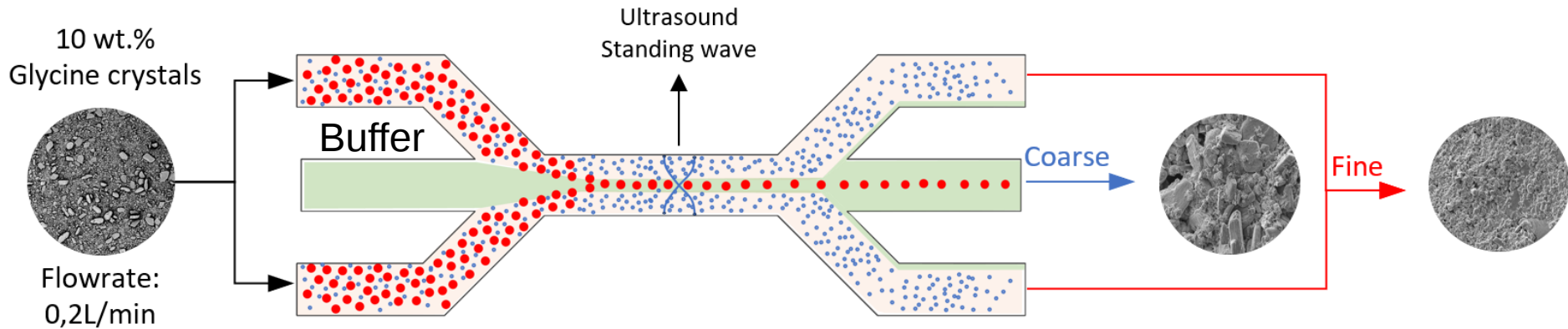
Solution: Peltier-based PID feedback controller

Acoustics - heating considerations



Infrared sensor

Acoustofluidic separation



Acoustic separation – high solid loads

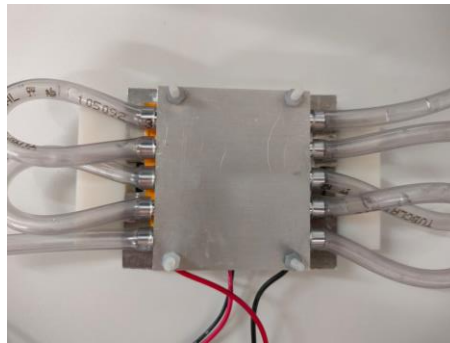
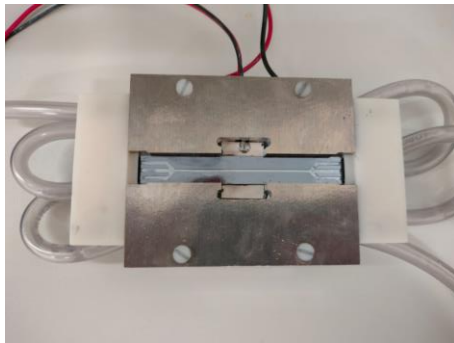
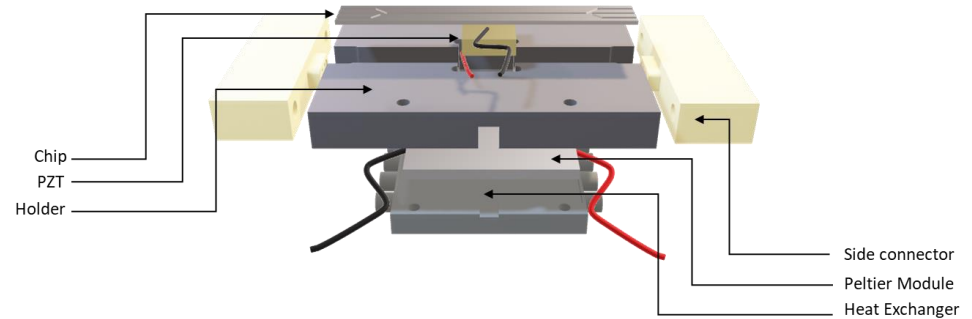
Process conditions:

Flowrate: 3.6 mL/min

Concentration: 10,0%

Potential: 240 V

Temperature: 30°C



Stability of separation tested up to
24 mins
(vial empty)

Acoustic separation – high solid loads

Process conditions:

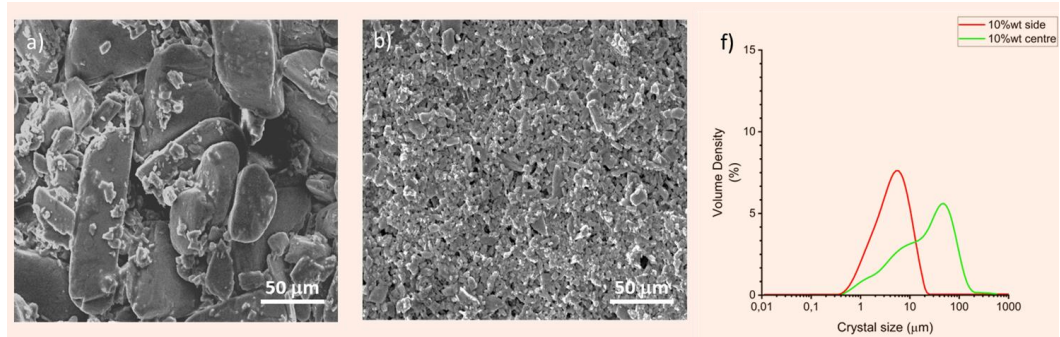
Flowrate: 3.6 mL/min

Concentration: 10,0%

Potential: 240V

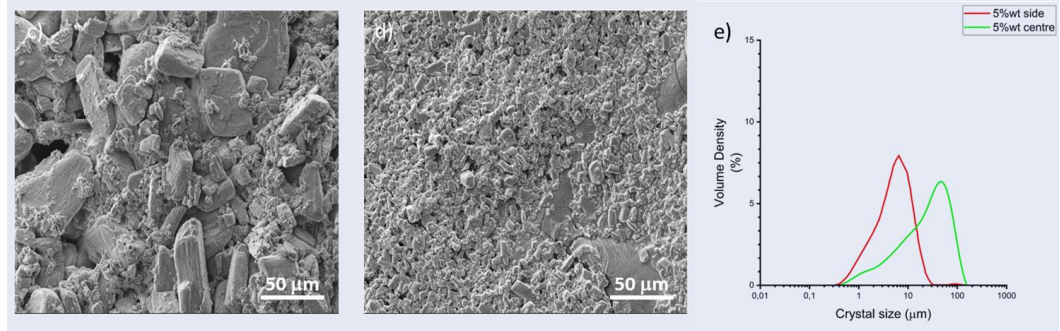
Temperature: 30°C

5%
solid load



Separation confirmed by SEM & Particle sizing

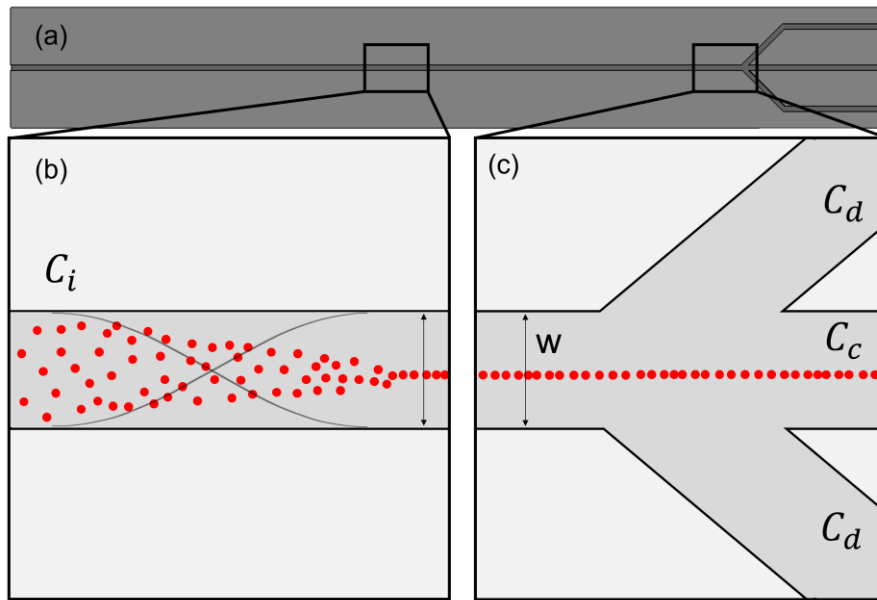
10%
solid load



center

side

Increase of cell suspension concentration



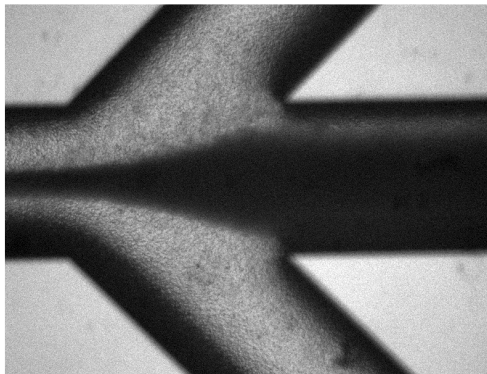
$$F_{rad} = 4\pi k \Phi a^3 E_{ac} \sin(2yk + \pi)$$

$$\text{Concentration factor: } F_c = \frac{C_c}{C_i}$$

Saccharomyces cerevisiae (Yeast),
 10^9 cells/ml

Increase of cell suspension concentration

Saccharomyces cerevisiae



Cells	Chip height (μm)	Potential (mV)	Cell volume content (%)	Cells/ml	Flow* (mg/min)	Fc
Yeast	250 μm	200	7,06	2.65*10 ⁸	15	2,94
			14,11	5.30*10 ⁸		2,22
			70,57	2.65*10 ⁹		1,27
	435μm	400	14,11	5.30*10 ⁸	50	1,99
		800			100	1,64
					50	2,73
					100	1,74

*1g considered as 1 ml

Parameters:

- Chip height
- Potential
- Solid content
- Cell initial concentration (solid content)
- Flow

Conclusions

- Laminar flows
 - Great, but not always...
 - Increasing channel sizes: diffusion limitations gain importance
 - Taylor-Aris dispersion reduces concentration, increases spreading and flow heterogeneity
 - Novel emerging lateral flow methodologies can address this
- Increasing throughput
 - Flow distribution critical
 - Enhancing (lateral) mass transport essential
 - Particles size determines whether particles focus
 - 2.5 D $\rightarrow$ 3D organization increases attainable throughput
- Many opportunities with (structured) preactors
- Limited applications in industry, due to:
 - Low throughput
 - Fouling
 - Unknown technology